

BS EN ISO 6892-1:2009

BS British Standard

Metallic materials ☒ Tensile testing

Part 1: Method of test at ambient temperature

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British Standard worldwide™

BSi
British Standards

National foreword

This British Standard is the UK implementation of EN ISO 6892-1:2009. It supersedes BS EN 10002-1:2001 which is withdrawn.

The UK participation in its preparation was entrusted by Technical Committee ISE/NFE/4, Mechanical testing of metals, to Subcommittee ISE/NFE/4/1, Uniaxial testing of metals.

A list of organizations represented on this committee can be obtained on request to its secretary.

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roo te erature (SO 6892-1:2 9)

Matér aux étall que - E a de tra to - Parte 1:
Mét ode d'e a à te érature a ba te (SO 6892-
1:2 9)

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Foreword

This document (EN SO 6892-1:2 9) has been prepared by Technical Committee SO/TC 164 "Mechanical test methods" in collaboration with Technical Committee EC SS/TC 1 "Telecommunications" of the European Committee for Standardization (CEN) and the Association of French Standardization (AFNOR).

This European Standard shall be given the status of a national standard, either by publication or by endorsement, at the latest by February 2 1, and all national standards shall be withdrawn at the latest by February 2 1.

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This document (EN SO 6892-1:2 9) has been approved by CEN as a European Standard (EN SO 6892-1:2 9) without any modification.

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Foreword

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ISO 6892-1 was prepared by Technical Committee ISO/TC 164, Mechanical testing of metals, Subcommittee SC 1, Uxial tests.

This document is identical to ISO 6892-1 as published in 1998.

ISO 6892 consists of the following parts, under the general title *Metallic materials — Tensile tests*:

— Part 1: *Method of test at room temperature*

The following parts are under preparation:

— Part 2: *Method of test at elevated temperature*

— Part 3: *Method of test at low temperature*

The following part is planned:

— Part 4: *Method of test in liquid helium*

Introduction

During the period of the preparation of SO 6892:1998, two methods for the determination of the rate of rotation were proposed.

In part of SO 6892, there are two methods of test available. The first, method A, based on the rate of change of the angular velocity and the second, method B, based on the rate of change of the angular displacement. The test results obtained by the two methods are determined by the accuracy of the test results.

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Metals — Tensile test —

Part 1:

Method of test at room temperature

1 Scope

This part of ISO 6892 describes the method of tensile test of metallic materials at room temperature.

NOTE A detailed table of relevant references is available in the annex.

2 Normative references

The following references are deemed to be applicable in full. For dated references, only the edition cited applies. For undated references, the latest edition of the referenced document (including any amendments) applies.

ISO 377, *Steel and steel products — Load and deformation characteristics of steel bars*

ISO 2566-1, *Steel — Conversion of carbon content — Part 1: Carbon and low alloy steel*

ISO 2566-2, *Steel — Conversion of carbon content — Part 2: Austenitic steel*

ISO 75-1, *Metals — Determination of tensile strength — Part 1: Test of round bars — Determination of tensile strength*

ISO 9513, *Metals — Calibration of extensometers used in tensile test*

3 Terms and definitions

For the purpose of this document, the following terms apply.

3.1

gauge length

L

length of the parallel portion of the test piece over which the elongation is measured at any one time during the test

ISO/TR 25679:2015³

3.1.1

original gauge length

L_0

length between gauge length (3.1) marks of the specimen measured at room temperature before the test

NOTE Adapted from ISO/TR 25679:2015³.

3.1.2

al au e le t a ter ru ture
al au e le t a ter ra ture

L_u
le t betwee au e le t (3.1) ark o t e t e e ea ured a ter ru ture, at roo te erature, t e
two ee av beee are ully tted bak to et er ot att er axe le a tra tle

NOTE Ada ted ro SO/TR 25679:2 5³.

3.2

arallel le t

L
le t o t e arallel redu ed e to o t e t e e e

SO/TR 25679:2 5³

NOTE Te o e t o arallel le t re la ed by t e o e t o d ta e betwee r ro u a ed te t
e e .

3.3

elo ato

rea e t e or al au e le t (3.1.1) at a y o e t dur t e t e t

NOTE Ada ted ro SO/TR 25679:2 5³.

3.4

er e ta e elo ato

elo ato ex re ed a a er e ta e o t e or al au e le t , L_o (3.1.1)

SO/TR 25679:2 5³

3.4.1

er e ta e er a e t elo ato

rea e t e or al au e le t (3.1.1) o a t e t e e a ter re oval o a e ed tre , ex re ed a
a er e ta e o t e or al au e le t , L_o

SO/TR 25679:2 5³

3.4.2

er e ta e elo ato a ter ra ture

A
er a e t elo ato o t e au e le t a ter ra ture, ($L_u - L_o$), ex re ed a a er e ta e o t e or al
au e le t , L_o

SO/TR 25679:2 5³

NOTE For ro orto al te t e e , t e or al au e le t ot equ vale t to $5,65\sqrt{S_o}$ ¹⁾ were S_o t e
or al ro - e to al area o t e arallel le t , t e y bol A ould be u le e ted by a ub r t d at t e
oe e to ro orto al ty u ed, e. . $A_{11,3}$ d ate a er e ta e elo ato o t e au e le t , L_o , o

$$A_{11,3} = 11,3\sqrt{S_o}$$

For o - ro orto al te t e e (ee A ex B), t e y bol A ould be u le e ted by a ub r t d at t e
or al au e le t u ed, ex re ed ll etre , e. . A_g d ate a er e ta e elo ato o a au e le t , L_o ,
o 8 .

1) $5,65\sqrt{S_o} = r_{\sqrt{1 + \cos(\pi)}}$.

3.5

exte o eter au ele t

L_e
tal exte o eter au ele t ued or ea ure e to exte o by ea o a exte o eter

NOTE 1 Ada ted ro SO/TR 25679:2 5³.

NOTE 2 For ea ure e to yeld a d roo tre t ara eter, L_e ould a a u o te arallel le t o te te t e e a o ble. deally, a a u, L_e ould be reater ta ,5 L_o but le t a a rox ately ,9 L . T ould e ure t at te exte o eter dete t all yeld eve t t at o ur t e t e e. Furt er, or ea ure e to ara eter "at" or "a ter rea " ax u or e, L_e ould be a rox ately equal to L_o .

3.6

exte o

rea e t e exte o eter au ele t, L_e (3.5), at a y o e t dur t e t e t

SO/TR 25679:2 5³

3.6.1

er e ta e exte o

" tra "

exte o ex re ed a a er e ta e o t e exte o eter au ele t, L_e (3.5)

3.6.2

er e ta e er a e t exte o

rea e t e exte o eter au ele t, a ter re oval o a e ed tre ro t e t e t e e, ex re ed a a er e ta e o t e exte o eter au ele t, L_e (3.5)

SO/TR 25679:2 5³

3.6.3

er e ta e yeld o t exte o

A_e
d o t uou yeld ateral, t e exte o betwee t e tart o yeld a d t e tart o u or work arde, ex re ed a a er e ta e o t e exte o eter au ele t, L_e (3.5)

NOTE Ada ted ro SO/TR 25679:2 5³.

See F ure 7.

3.6.4

er e ta e total exte o at ax u or e

A_t
total exte o (ela t exte o lu la t exte o) at ax u or e, ex re ed a a er e ta e o t e exte o eter au ele t, L_e (3.5)

See F ure 1.

3.6.5

er e ta e la t exte o at ax u or e

A
la t exte o at ax u or e, ex re ed a a er e ta e o t e exte o eter au ele t, L_e (3.5)

See F ure 1.

3.6.6

er e ta e total exte o at ra ture

A_t
 total exte o (ela t exte o lu la t exte o) at t e o e to ra ture, ex re ed a a er e ta e o t e exte o eter au e le t , L_e (3.5)

See F ure 1.

3.7 Te t rate

3.7.1

tra rate

\dot{e}_{L_e}

rea e o tra , ea ured wt a exte o eter, **exte o eter au e le t** , L_e (3.5), ert e

NOTE See 3.5.

3.7.2

e t ated tra rate over t e arallel le t

\dot{e}_L

value o t e rea e o tra over t e **arallel le t** , L (3.2), o t e t e t e e ert e ba ed o t e **ro ead e arat o rate** (3.7.3) a d t e arallel le t o t e t e e

3.7.3

ro ead e arat o rate

v

d la e e t o t e ro ead ert e

3.7.4

tre rate

\dot{R}

rea e o tre ert e

NOTE Stre rate ould o ly be u ed t e ela t ar t o t e t (et od B).

3.8

er e ta e redu t o o area

ax u a e ro - e to al area w a o urred dur t e t e t , $(S_o - S_u)$, ex re ed a a er e ta e o t e or al ro - e to al area, S_o :

$$= \frac{S_o - S_u}{S_o} \times 1$$

3.9 Max u ore

NOTE For ateral w d lay d o t uou yeld , but w ere o work arde a be e tabl ed, F ot de ed t ar t o SO 6892 ee oot o te to F ure 8).

3.9.1

ax u ore

F

(ateral d lay o d o t uou yeld) e t or e t at t e t e e wt ta d dur t e t e t

3.9.2

ax u or e

F

< lateral d lay d o t uou yeld > e t o r e t a t t e t e t e e w t t a d d u r t e t e t a t e r t e b e o w o r k a r d e

NOTE See F ure 8 a) a d b).

3.1

tre

a t a y o e t d u r t e t e t, o r e d v d e d b y t e o r a l r o - e t o a l a r e a, S_0 , o t e t e t e e

NOTE 1 A d a t e d r o S O / T R 2 5 6 7 9 : 2 5³.

NOTE 2 A l l r e r e e t o t r e t a r t o S O 6 8 9 2 a r e t o e e e r t r e .

NOTE 3 w a t f o l l o w , t e d e a t o " o r e " a d " t r e " o r " e x t e o ", " e r e t a e e x t e o " a d " t r a ", r e e t v e l y, a r e u e d o v a r o u o a o (a u r e a x l a b e l o r e x l a t o o r t e d e t e r a t o o d e r e t r o r t e). H o w e v e r, o r a e r a l d e r t o o r d e t o o a w e l l - d e e d o t o a u r v e, t e d e a t o " o r e " a d " t r e " o r " e x t e o ", " e r e t a e e x t e o " a d " t r a ", r e e t v e l y, a r e t e r a e a b l e.

3.1 .1

te le tre t

R

t r e o r r e o d t o t e a x u o r e, *F* (3.9)

SO/TR 25679:2 5³

3.1 .2

yeld tre t

w e t e e t a l l a t e r a l e x b t a y e l d e o e o, t r e o r r e o d t o t e o t r e a e d d u r t e t e t a t w l a t d e o r a t o o u r w t o u t a y r e a e t e o r e

NOTE A d a t e d r o S O / T R 2 5 6 7 9 : 2 5³.

3.1 .2.1

u er yeld tre t

R_{eH}

a x u v a l u e o t r e (3 . 1) r o r t o t e r t d e r e a e o r e

NOTE A d a t e d r o S O / T R 2 5 6 7 9 : 2 5³.

See F ure 2.

3.1 .2.2

lower yeld tre t

R_{eL}

l o w e t v a l u e o t r e (3 . 1) d u r l a t y e l d, o r a y t a l t r a e t e e t

SO/TR 25679:2 5³

See F ure 2.

3.1 .3

root re t , la t exte o

R
tre atw t e la t exte o equal to a e ed er e ta e o t e exte o eter au e le t , L_e
(3.5)

NOTE 1 Ada ted ro SO/TR 25679:2 5, " roo tre t , o - ro orto al exte o".

NOTE 2 A u x added to t e ub r t to d at e t e re r bed er e ta e, e. . R_{2} .

See F ure 3.

3.1 .4

root re t , total exte o

R_t
tre atw total exte o (ela t exte o lu la t exte o) equal to a e ed er e ta e o
t e exte o eter au e le t , L_e (3.5)

NOTE 1 Ada ted ro SO/TR 25679:2 5³.

NOTE 2 A u x added to t e ub r t to d at e t e re r bed er e ta e, e. . R_t , 5.

See F ure 4.

3.1 .5

er a e t et tre t

R_r
tre atw , a ter re oval o or e, a e ed er a e t e lo ato or exte o , ex re ed re e t vely
a a er e ta e o or al au e le t , L_o (3.1.1), or exte o eter au e le t , L_e (3.5), a ot bee
ex eeded

SO/TR 25679:2 5³

See F ure 5.

NOTE A u x added to t e ub r t to d at e t e e ed er e ta e o t e or al au e le t , L_o , or o t e
exte o eter au e le t , L_e , e. . R_r , 2.

3.11

ra ture

e o e o w dee ed to o ur w e total e arato o t e t e e o ur

NOTE Crtera or ra ture w ay be u ed or o uter o trolle t e t are ve F ure A.2.

4 Ter a d y bol


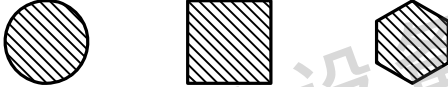
T e y bol u ed t art o SO 6892 a d orre o d de at o are ve Table 1.

Table 1 — Sy bol a d de at o

Sy bol	U t	De at o
T e t e e		
a_o, T^a		or al t k e o a lat te t e e or wall t k e o a tube
b_o		or al wdt o t e arallel le t o a lat te t e e or avera e wdt o t e lo tud al tr take ro a tube or wdt o lat wre
d_o		or al d a eter o t e arallel le t o a r ular te t e e, or d a eter o rou d wre or ter al d a eter o a tube
D_o		or al exter al d a eter o a tube
L_o		or al au e le t
L'_o		t al au e le t or deter at o o A_w (ee A ex)
L		arallel le t
L_e		exte o eter au e le t
L_t		total le t o te t e e
L_u		al au e le t a ter ra ture
L'_u		al au e le t a ter ra ture or deter at o o A_w (ee A ex)
S_o	2	or al ro - e to al area o t e arallel le t
S_u	2	u ro - e to al area a ter ra ture
k	—	oe e to ro orto al ty (ee 6.1.1)
	%	er e ta e redu to o area
Elo at o		
A	%	er e ta e elo at o a ter ra ture (ee 3.4.2)
A_w	%	er e ta e la t elo at o wt out e k (ee A ex)
Exte o		
A_e	%	er e ta e yeld o t exte o
A	%	er e ta e la t exte o at ax u or e, F
A_t	%	er e ta e total exte o at ax u or e, F
A_t	%	er e ta e total exte o at ra ture
ΔL		exte o at ax u or e
ΔL		exte o at ra ture
Rate		
$\dot{\epsilon}_{L_e}$	-1	tra rate
$\dot{\epsilon}_L$	-1	e t ated tra rate over t e arallel le t
\dot{R}	MPa ⁻¹	tre rate
v	-1	ro ead e arato rate

Table 2 — Ma ty e o te t e e a ord to rodu t ty e

D e o l l etre

Ty e o rodu t		Corre o d A ex
<p>S eet — Plate — Flat</p>  <p>T k e a</p>	<p>W re — Bar — Se to</p>  <p>D a eter or de</p>	
$,1 \leq a < 3$	—	B
—	< 4	C
$a \geq 3$	≥ 4	D
Tube		E

6.3 Pre arat o o te t e e

T e te t e e all be take a d re ared a orda e wt t e require e t o t e releva t ter at o al Sta dard ort e d e re t ateral (e. . SO 377).

7 Deter ato o or al ro - e t o al area

T e releva t d e o o t e t e e ould be ea ured at u e t ro - e t o er e d ular to t e lo tud al ax t e e tral re o o t e arallel e t o t e t e e.

A u o t ree ro - e t o re o e ded.

T e or al ro - e t o al area, S_0 , t e a vera e ro - e t o al area a d all be al ulated ro t e ea ure e t o t e a ro rated e o .

T e a ura y o t al ulato de e d o t e ature a d ty e o t e t e e. A ex e B to E de r be et o d ort e evaluato o S_0 or d e re t ty e o t e t e e a d o t a e ato ort e a ura y o ea ure e t.

8 Mark t e or al au e le t

Ea e d o t e or al au e le t, L_0 , all be arked by ea o e ark or r bed l e , but ot by ot e w ould re ult re ature ra ture.

For ro ort o al te t e e , t e al ulated value o t e or al au e le t ay be rou ded to t e ea re t ult le o 5 , rov ded t at t e d e re e betwee t e al ulated a d arked au e le t le t a 1 % o L_0 . T e or al au e le t all be arked to a a ura y o $\pm 1\%$.

t e arallel e t, L , u reater t a t e or al au e le t, a , or t a e, wt u a ed te t e e , a ere o overla au e le t ay be arked.

o e a e , t ay be el ul to draw, o t e ura e o t e t e e , a l e arallel to t e lo tud al ax , alo w t e au e le t are arked.

9 A ura y o te t a aratu

T e o r e - e a u r y t e o t e t e t a e a l l b e a l b r a t e d a o r d a e w t S O 7 5 - 1, l a 1, o r b e t t e r .

F o r t e d e t e r a t o o r o o t r e t (l a t o r t o t a l e x t e o) t e u e d e x t e o e t e r a l l b e a o r d a e w t S O 9 5 1 3, l a 1 o r b e t t e r, t e r e l e v a t r a e . F o r o t e r r o e r t e (w t e r e x t e o) a S O 9 5 1 3, l a 2 e x t e o e t e r t e r e l e v a t r a e a y b e u e d .

1 C o d t o o t e t

1 . 1 S e t t t e o r e z e r o o t

T e o r e - e a u r y t e a l l b e e t t o z e r o a t e r t e t e t l o a d t r a a b e e a e b l e d, b u t b e o r t e t e t e e a t u a l l y r e d a t b o t e d . O e t e o r e z e r o o t a b e e e t, t e o r e - e a u r y t e a y o t b e a e d a y w a y d u r t e t e t .

N O T E T e u e o t e t o d e u r e, t a t o o e a d t e w e t o t e r y t e o e a t e d o r t e o r e e a u r e e t a d o t e o t e r a d a y o r e r e s u l t r o t e l a o e r a t o d o e o t a e t t e a u r e e t .

1 . 2 M e t o d o r

T e t e t e e a l l b e r e d b y u t a b l e e a, u a w e d e, r e w e d r, a r a l l e l a w a e, o r o u l d e r e d o l d e r .

E v e r y e d e a v o u r o u l d b e a d e t o e u r e t a t t e e e a r e e l d u a w a y t a t t e o r e a l e d a a x a l l y a o b l e, o r d e r t o z e b e d (o r e o r a t o v e A S T M E 1 1 2⁸, o r e x a l e). T o o a r t u l a r o r t a e w e t e t b r i t t l e a t e r a l o r w e d e t e r r o o t r e t (l a t e x t e o), r o o t r e t (t o t a l e x t e o) o r y e l d t r e t .

o r d e r t o o b t a a t r a t t e t e e a d e u r e t e a l e t o t e t e t e e a d r a r a e e t, a r e l a r y o r e a y b e a l e d r o v d e d t d o e o t e x e e d a v a l u e o r r e o d t o 5 % o t e e e d o r e x e t e d y e l d t r e t .

A o r r e t o o t e e x t e o o u l d b e a r r e d o u t t o t a k e t o a o u t t e e e t o t e r e l a r y o r e .

1 . 3 T e t r a t e b a e d o t r a t e o t r o l (e t o d A)

1 . 3 . 1 G e r a l

M e t o d A t e d e d t o z e t e v a r a t o o t e t e t r a t e d u r t e o e t w e t r a t e e t v e a r a e t e r a r e d e t e r e d a d t o z e t e e a u r e e t u e r t a t y o t e t e t r e u l t .

T w o d e r e t t y e o t r a t e o t r o l a r e d e r b e d t e t o . T e r t t e o t r o l o t e t r a t e t e l, $\dot{\epsilon}_{L_e}$, t a t b a e d o t e e e d b a k o b t a e d r o a e x t e o e t e r . T e e o d t e o t r o l o t e e t a t e d t r a t e o v e r t e a r a l l e l l e t, $\dot{\epsilon}_L$, w a e v e d b y o t r o l l t e r o e a d e a r a t o r a t e a t a v e l o t y e q u a l t o t e d e r e d t r a t e u l t l e d b y t e a r a l l e l l e t .

a a t e r a l o w o o e e o u d e o r a t o b e a v o u r a d t e o r e r e a o a l l y o t a t t e t r a t e, $\dot{\epsilon}_{L_e}$, a d t e e t a t e d t r a t e o v e r t e a r a l l e l l e t, $\dot{\epsilon}_L$, a r e a r o x a t e l y e q u a l . D e r e e e x t t e a t e r a l e x b t d o t o u o r e r r a t e d y e l d (e . . o e t e e l a d A I M a l l o y t e y e l d o t e l o a t o r a e, o r a t e r a l w o w e r r a t e d y e l d l i k e t e P o r t e v - L e C a t e l e r e e t) o r

ekour. teore rea , te et ated tra rate ay be ub ta tally below t e tar et tra rate due to t e o la e o t e t e t a e.

T e t e t rate all o or to t e ollow require e t .

a) t e ra e u to a d lud t e deter ato o R_{eH} , R or R_t , t e e ed tra rate, $\dot{\epsilon}_{L_e}$ (ee 3.7.1), all be a led. t ra e, to el at e t e lue e o t e o la e o t e t e l e t e a e, t e u e o a exte o eter la ed o t e t e t e e e e ary to ave a urate o trol over t e tra rate. (For t e t a e u able to o trol by tra rate, a ro edure u t e e t ated tra rate over t e arallel le t , $\dot{\epsilon}_L$, ay be u ed.)

b) Dur d o t uou yeld , t e e t ated tra rate over t e arallel le t , $\dot{\epsilon}_L$ (ee 3.7.2), ould be a led. t ra e, t o ble to o trol t e tra rate u t e exte o eter la ed o t e t e t e e be au e lo al yeld a o ur out de t e exte o eter au e le t . T e requ red e t ated tra rate over t e arallel le t ay be a ta ed t ra e u e tly a urately u a o ta t ro ead e arato rate, v (ee 3.7.3);

$$v = L \dot{\epsilon}_L \tag{1}$$

w ere

$\dot{\epsilon}_L$ t e e t ated tra rate over t e arallel le t ;

L t e arallel le t .

) t e ra e ollow R or R_t or e d o yeld (ee 3.7.2), $\dot{\epsilon}_{L_e}$ or $\dot{\epsilon}_L$ a be u ed. T e u e o $\dot{\epsilon}_L$ re o e ded to avo d a y o trol robe w ay ar e e k o ur out de t e exte o eter au e le t .

T e tra rate e ed 1.3.2 to 1.3.4 all be a ta ed dur t e deter ato o t e releva t ateral ro erty (ee al o F ure 9).

Dur wt to a o t er tra rate or to a o t er o trol ode, o d o t ute t e tre - tra urve ould be tro du ed w d tort t e value o R , A or A_t (ee F ure 1). T e e t a be redu ed by a u table radual wt betwee t e rate .

T e a e o t e tre - tra urve t e work arde ra e a al o be lue ed by t e tra rate. T e t e t rate u ed ould be do u e ted (ee 1 .6).

1.3.2 Stra rate or t e deter ato o t e u er yeld tre t , R_{eH} , or roo tre t ro erte , R , a d R_t

T e tra rate, $\dot{\epsilon}_{L_e}$, all be ke t a o ta t a o ble u to a d lud t e deter ato o R_{eH} or R or R_t . Dur t e deter ato o t e e ateral ro erte t e tra rate, $\dot{\epsilon}_{L_e}$, all be o e o t e two ollow e ed ra e (ee al o F ure 9).

Ra e 1: $\dot{\epsilon}_{L_e} =$, 7^{-1} , wt a relat ve tolera e o ± 2 %

Ra e 2: $\dot{\epsilon}_{L_e} =$, 25^{-1} , wt a relat ve tolera e o ± 2 % (re o e ded u le o t erw e e ed)

t e t e t a e o t able to o trol t e tra rate d re tly, t e e t ated tra rate over t e arallel le t , $\dot{\epsilon}_L$, e. o ta t ro ead e arato rate, all be u ed. T rate all be al ulated u Equato (1).

The ultimate tensile strength will be lower than the yield strength but the elongation at break will be higher. A detailed explanation is given in Annex F.

1.3.3 Strain rate or the determination of the lower yield strength, R_{eL} , and the yield point extension, A_e

Following the determination of the upper yield strength (see A.4.2), the determined strain rate over the parallel length, $\dot{\epsilon}_L$, shall be adjusted to one of the following two standard rates (see Figure 9) until the yield point is reached.

Rate 2: $\dot{\epsilon}_L = 0,25 \text{ s}^{-1}$, with a relative tolerance of $\pm 2 \%$ (recommended, when R_{eL} determined)

Rate 3: $\dot{\epsilon}_L = 2 \text{ s}^{-1}$, with a relative tolerance of $\pm 2 \%$

1.3.4 Strain rate or the determination of the tensile strength, R , and the elongation at break, A , and the total extension at the maximum force, A_T , and the lateral extension at maximum force, A , and the reduction of area,

At the determination of the required yield/proof strength ratio, the determined strain rate over the parallel length, $\dot{\epsilon}_L$, shall be adjusted to one of the following standard rates (see Figure 9).

Rate 2: $\dot{\epsilon}_L = 0,25 \text{ s}^{-1}$, with a relative tolerance of $\pm 2 \%$

Rate 3: $\dot{\epsilon}_L = 2 \text{ s}^{-1}$, with a relative tolerance of $\pm 2 \%$

Rate 4: $\dot{\epsilon}_L = 6,7 \text{ s}^{-1}$, with a relative tolerance of $\pm 2 \%$ ($0,4 \text{ s}^{-1}$, with a relative tolerance of $\pm 2 \%$) (recommended unless otherwise specified)

The upper yield strength is only determined if the tensile strength, the determined strain rate over the parallel length of the test piece is 3 or 4 may be allowed throughout the test.

1.4 Test rate based on the rate (set of B)

1.4.1 General

The test rate shall conform to the following requirements determined by the nature of the material. Unless otherwise specified, any of the test rates may be used up to a rate equivalent to the upper yield strength. The test rate above the yield point is not recommended.

1.4.2 Yield and proof strength

1.4.2.1 Upper yield strength, R_{eH}

The rate of the ratio of the load to the area shall be kept constant throughout the test. The test rate is given in Table 3.

NOTE For wrought, typical lateral average elongation of elasticity shall be 15 MPa (including the alloy, brass, and titanium). Typical lateral average elongation of elasticity shall be 15 MPa (including wrought steel, titanium, and nickel-based alloy).

Table 3 — Str rate

Modulu o elat ty o t e ater al E MPa	Stre rate \dot{R} MPa ⁻¹	
	.	ax.
< 15	2	2
≥ 15	6	6

1.4.2.2 Lower yeld tre t , R_{eL}

o ly t e lower yeld tre t be deter ed, t e tra rate dur yeld o t e arallel le t o t e t e e e all be betwe , 25^{-1} a d , 25^{-1} . T e tra rate wt t e arallel le t all be ke t a o t a t a o ble. t rate a o t be re ulat d re tly, t all be xed by re ulat t e tre rate u t be ore yeld be , t e o trol o t e a e o t be urt er ad u ted u t l o l e t o o yeld.

o a e all t e tre rate t e elat ra e ex eed t e ax u rate ve Table 3.

1.4.2.3 U er a d lower yeld tre t , R_{eH} a d R_{eL}

bot u er a d lower yeld tre t are deter ed dur t e a e t e t t e o d t o r deter t e lower yeld tre t all be o led wt (ee 1.4.2.2).

1.4.2.4 Proo tre t (la t exte o) a d roo tre t (total exte o), R a d R_t

T e rate o e arat o t e ro ead o t e a e all be ke t a o t a t a o ble a d wt t e l t orre o d t o t e tre rate Table 3 wt t e elat ra e.

Wt t e la t ra e a d u t o t e roo tre t (la t exte o or total exte o), t e tra rate all o t ex eed , 25^{-1} .

1.4.2.5 Rate o e arat o

t e t e t a e o t a able o ea ur or o trol t e tra rate, a ro ead e arat o rate equ vale t t o t e tre rate ve Table 3 all be u ed u t l o l e t o o yeld.

1.4.2.6 Te le tre t , R , er e ta e elo at o a ter ra ture, A , er e ta e total exte o at t e ax u or e, A_t , er e ta e la t exte o at ax u or e, A , a d er e ta e redu t o area,

A ter deter at o o t e requ red yeld/ roo tre t ro erte , t e t e t rate ay be rea ed to a tra rate (or equ vale t ro ead e arat o rate) o reater t a , 8^{-1} .

o ly t e te le tre t o t e ater al t o be ea ured, a le tra rate a be u ed t rou out t e te tw all o t ex eed , 8^{-1} .

1.5 C o e o t e et od a d rate

U le o t er w e a reed, t e o e o et od (A or B) a d t e t rate are at t e d re t o o t e rodu er or t e t e t laboratory a ed by t e rodu er, rov ded t at t e e e e t t e requ re e t o t art o SO 6892.

1.6 Do u e t a t o o t e o e t e t o d t o

order to report the test control mode and test rate as abbreviated or, the following symbols are abbreviated as follows:

SO 6892 A, or SO 6892 B

where 'A' denotes the test mode of A (test rate control), and 'B' denotes the test mode of B (test rate based). The symbols '1' and '2' are a reference to 3 parameters that refer to the test rate used during each test, as defined in Figure 9, and '1' may be added to designate the test rate (MPa^{-1}) selected during each load.

EXAMPLE 1 SO 6892-1:2 9 A224 denotes a test based on test rate control, using rate 2, 2 and 4.

EXAMPLE 2 SO 6892-1:2 9 B3 denotes a test based on test rate, performed at a nominal test rate of 3 MPa^{-1} .

EXAMPLE 3 SO 6892-1:2 9 B denotes a test based on test rate, performed at a nominal test rate according to Table 3.

11 Determination of the upper yield strength

R_{eH} may be determined from the stress-strain curve or peak load divided by the maximum value of the force divided by the area or the latter obtained by dividing the force by the original cross-sectional area of the test piece, S_0 (see Figure 2).

12 Determination of the lower yield strength

R_{eL} determined from the stress-strain curve and divided by the lowest value of the derivative, or a yield point test. The latter obtained by dividing the force by the original cross-sectional area of the test piece, S_0 (see Figure 2).

For rod type test pieces, R_{eL} may be reported as the lowest test weight per unit length, 25% greater than R_{eH} , or taken to a satisfactory test piece. After determining R_{eL} by the procedure, the test rate may be read as per 1.3.4. Under the order procedure could be re-ordered to the test report.

NOTE The ultimate tensile strength A_e should be determined.

13 Determination of the proof stress, the extension

13.1 R_p determined from the stress-strain curve by drawing a line parallel to the linear portion of the curve and at a distance equivalent to the required percentage extension, e.g., 2%. The test at which the test piece yields or the order of the test is the proof stress. The latter obtained by dividing the force by the original cross-sectional area of the test piece, S_0 (see Figure 3).

The test portion of the stress-strain curve is clearly defined, thereby revealing the drawing parallel to the test piece, the following procedure is recommended (see Figure 6).

When the reduced proof stress is exceeded, the stress is reduced to a value equal to about 1% of the stress obtained. The stress is then read as a useful test value obtained normally. To determine the reduced proof stress, a line drawn through the yield point. All the drawing parallel to the line, at a distance of the order of the curve, is used along the axis, equal to the required percentage extension. The test portion of the stress-strain curve is clearly defined, thereby revealing the drawing parallel to the test piece, the following procedure is recommended (see Figure 6).

NOTE 1 Several methods may be used to determine the order of the force-extension curve. One of these is to plot the force parallel to the distance determined by the yield load on the force-extension curve. The other method is to plot the force parallel to the force-extension curve (see Figure 6).

NOTE 2 The latter method is only valid if the force-extension curve is linear. Start with a value of the force-extension curve at the yield load.

NOTE 3 The force-extension curve may be determined by the use of a rate of deformation control device.

13.2 The property may be obtained without the force-extension curve by using automatic device (see Annex A).

NOTE A further available method is described in GB/T 228¹².

14 Determination of the total extension

14.1 R_t determined on the force-extension curve, taking 1.2 into account, by drawing a line parallel to the ordinate axis (or the axis) and at a distance equivalent to the reduced total extension. The total width of the latter curve is the force-extension curve. The latter is obtained by dividing the force by the total area of the test piece, S_0 (see Figure 4).

14.2 The property may be obtained without the force-extension curve by using automatic device (see Annex A).

15 Method of verification of the test

The test piece is subjected to a force-extension curve for 1 to 12. The force is obtained by using the force-extension curve by the total area of the test piece, S_0 . After the force, the force is reduced to the force-extension curve or elongation of the test piece. The force is obtained by dividing the force by the total area, see Figure 5.

NOTE The value of the force-extension curve is the force-extension curve. The force is obtained by the force-extension curve. Example: Re = 75 MPa. The force is obtained by the force-extension curve. Example: Re = 75 MPa. The force is obtained by the force-extension curve. Example: Re = 75 MPa.

16 Determination of the yield point extension

For the total extension of the yield point, A_e determined on the force-extension curve by subtracting the extension at R_{eH} from the extension at the start of the work hardening. The extension at the start of the work hardening is determined by the force-extension curve, or to the work hardening curve (see Figure 7). The force is obtained by dividing the force by the total area, L_e .

The method used (see Figure 7 a) or b) should be described in the test report.

17 Determination of the force at maximum force

The method of determining the force at maximum force on the force-extension curve is obtained by subtracting the force at maximum force from the force at maximum force.

Calculate the error rate of the total extension at axial force, A , from Equation (2):

$$A = \left(\begin{matrix} \Delta L \\ L_e \quad E \end{matrix} \right) \times 1 \quad (2)$$

where

L_e is the extension of the element;

E is the modulus of elasticity of the test specimen;

R is the test force;

ΔL is the extension at axial force.

NOTE For lateral deflection of the test specimen, the error rate of the total extension at axial force is the extension of the test specimen, see Figure 1.

18 Determination of the error rate of the total extension at axial force

The method to determine the error rate of the total extension of the test specimen obtained with the extension of the test specimen.

Calculate the error rate of the total extension at axial force, A_t , from Equation (3):

$$A_t = \frac{\Delta L}{L_e} \times 1 \quad (3)$$

where

L_e is the extension of the element;

ΔL is the extension at axial force.

NOTE For lateral deflection of the test specimen, the error rate of the total extension at axial force is the extension of the test specimen, see Figure 1.

19 Determination of the error rate of the total extension at rate

The method to determine the error rate of the total extension of the test specimen obtained with the extension of the test specimen.

Calculate the error rate of the total extension at rate, A_t , from Equation (4):

$$A_t = \frac{\Delta L}{L_e} \times 1 \quad (4)$$

where

L_e is the extension of the element;

ΔL is the extension at rate.

2 Determination of wear rate at a temperature

2.1 Per e ta e elo ato a ter ra ture all be deter ed a orda ewt t e de to ve 3.4.2.

For t ur o e, t e two broke e e o t e t e e all be are ully tted ba k to et er o t at t er axe le a tra tle.

S e al re auto all be take to e ure ro er o ta t betwee t e broke art o t e t e e w e ea ur t e al au e le t . T art ularly orta t or t e t e e o all ro - e to a d t e t e e av low elo ato value .

Cal ulate t e er e ta e elo ato a ter ra ture, A , ro Equatio (5):

$$A = \frac{L_u - L_o}{L_o} \times 1 \quad (5)$$

w ere

L_o t e or al au e le t ;

L_u t e al au e le t a ter ra ture.

Elo ato a ter ra ture, $L_u - L_o$, all be deter ed to t e eare t ,25 or better u a ea ur dev ewt u e t re oluto .

t e e ed u er e ta e elo ato le t a 5%, t re o e ded t at e al re auto be take (ee A ex G). T e re ult o t deter ato val d o ly t e d ta e betwee t e ra ture a d t e eare t au e ark ot le t a $L_o/3$. However, t e ea ure e t val d, rre e t ve o t e o t o t e ra ture, t e er e ta e elo ato a ter ra ture equal to or reater t a t e e ed value.

2.2 W e exte o at ra ture ea ured u a exte o eter, t ot e e ary to ark t e au e le t . T e elo ato ea ured a t e total exte o at ra ture, a d t t ere ore e e ary to ded u t t e elat exte o or der to obta er e ta e elo ato a ter ra ture. To obta o arable value wt t e a ual et od, add to al adu t e t a be a led (e. . e ou dy a a d reque y ba dw dt o t e exte o eter, ee A.3.2).

T e re ult o t deter ato val d o ly ra ture a d lo alzed exte o (e k) o ur wt t e exte o eter au e le t , L_e . T e ea ure e t val d re ar dle o t e o t o t e ra ture ro - e to t e er e ta e elo ato a ter ra ture equal to or reater t a t e e ed value.

t e rodu t ta dard e e t e deter ato o er e ta e elo ato a ter ra ture or a ve au e le t , t e exte o eter au e le t ould be equal to t le t .

2.3 elo ato ea ured over a ve xed le t , t a be o verted to ro orto al au e le t , u o ver o or ulae or table a a reed be ore t e o e e e t o t e t (e. . a SO 2566-1 a d SO 2566-2).

NOTE Co ar o o er e ta e elo ato are o ble o ly w e t e au e le t or exte o eter au e le t , t e a ea d area o t e ro - e to are t e a e or w e t e oe e to ro orto alty, k , t e a e.

21 Determination of wear rate reduction area

Per e ta e redu to o area all be deter ed a orda ewt t e de to ve 3.8.

e e ary, t e two broke e e o t e t e e all be are ully tted ba k to et er o t at t er axe le a tra tle.

Calculate the error rate reduced to area, ϵ , from Equation (6):

$$\epsilon = \frac{S_o - S_u}{S_o} \times 100 \quad (6)$$

where

S_o is the total projected area of the parallel test;

S_u is the unprojected area at fracture.

Measure S_u to a accuracy of $\pm 2\%$ (see Figure 13).

NOTE Measure S_u with a accuracy of $\pm 2\%$ on all data after round test, or test the weight of error rate to avoid error, may not be possible.

22 Test report

The test report shall contain at least the following information to be agreed by the parties concerned:

- reference to the part of SO 6892 extended with the test method or standard, e.g. SO 6892-1:2 9 A224;
- description of the test piece;
 - specimen lateral, known;
 - type of test piece;
 - location and direction of the test piece, known;
 - test control mode () and test rate () or test rate range () (see 1.6) determined from the recorded test data value between 1.3 and 1.4;
 - test result.

Results should be rounded to the following requirements or better, not otherwise specified in the standard:

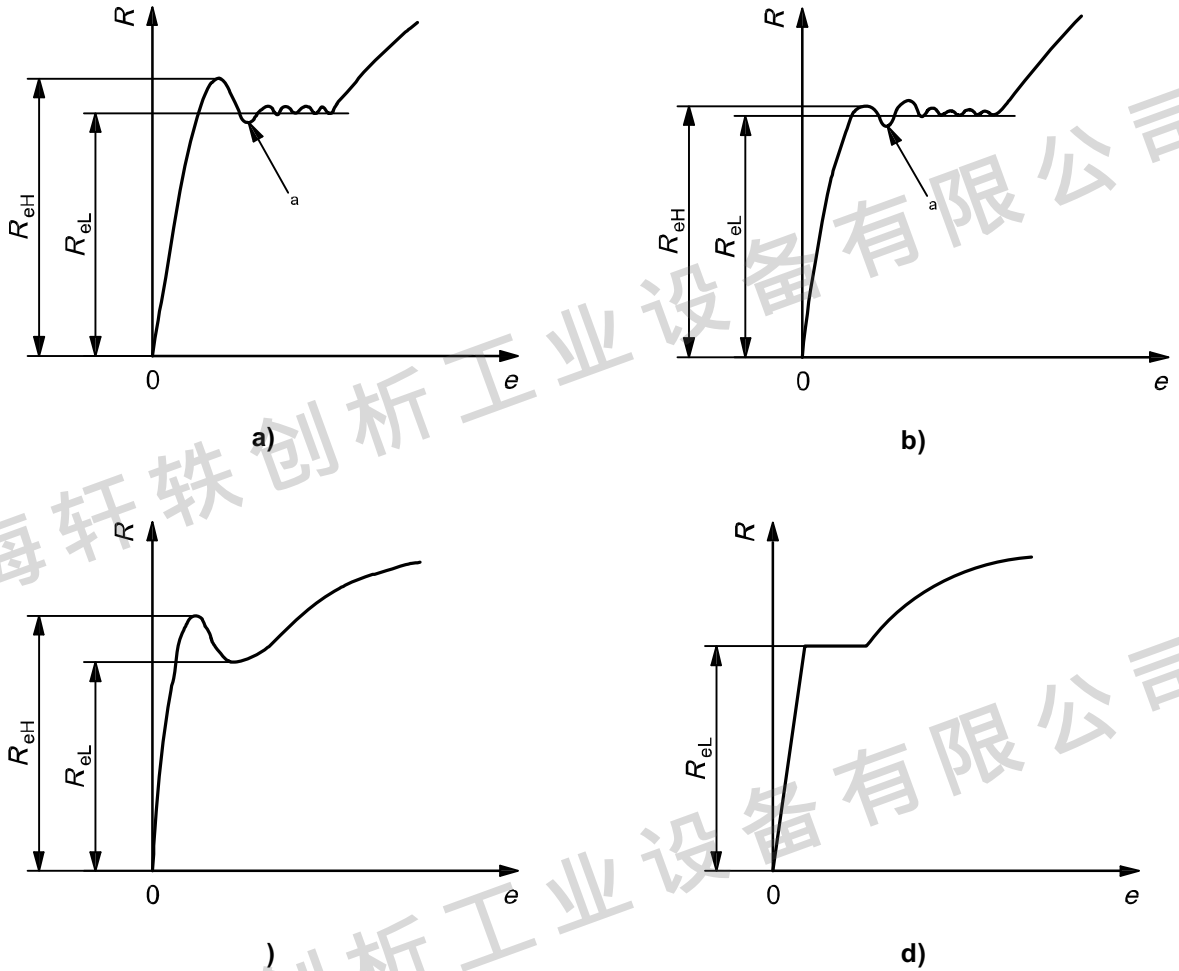
- test value, as a decimal, to the nearest whole number;
- error rate yield of test piece value, A_o , to the nearest 0.1%;
- all other error rate extended to a decimal value to the nearest 0.5%;
- error rate reduced to area, ϵ , to the nearest 1%.

23 Measure of uncertainty

23.1 General

Measure of uncertainty analysis is a useful tool for the assessment of the quality of measured results.

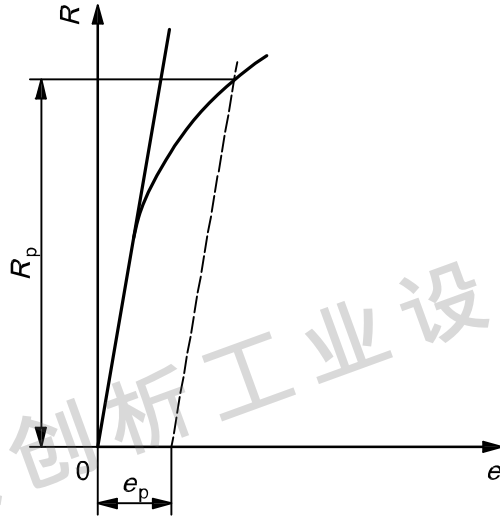
Product standard and material property data are based on the part of SO 6892 and earlier editions of SO 6892 have a reference to the error rate of the test piece. The test piece is a ratio to a length of the test piece or error rate of the test piece by the ratio of the test piece to the length. For the



Key

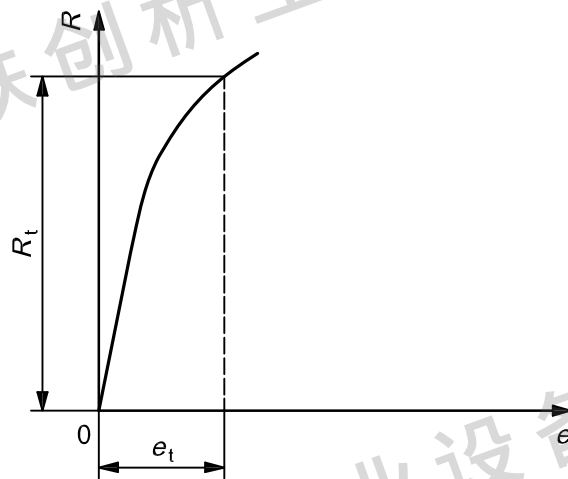
- e — strain
- R — stress
- R_{eH} — upper yield strength
- R_{eL} — lower yield strength
- a — total strain

Figure 2 — Example of upper and lower yield strength order type curve



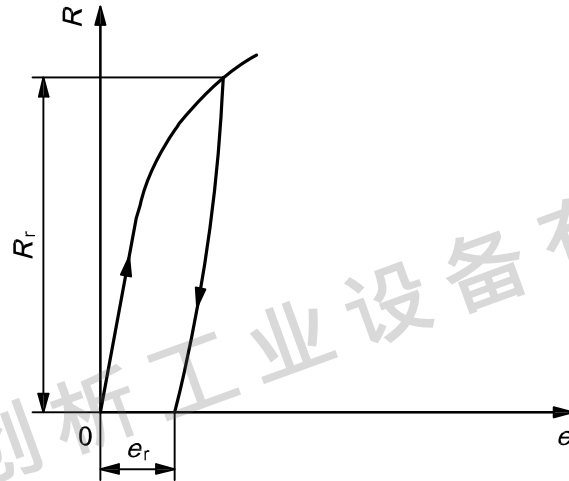
Key
 e permanent extension
 e_p permanent extension
 R force
 R_p proof stress, permanent extension

Figure 3 — Proof stress, permanent extension, R_p (see 13.1)



Key
 e permanent extension
 e_t permanent total extension
 R force
 R_t proof stress, total extension

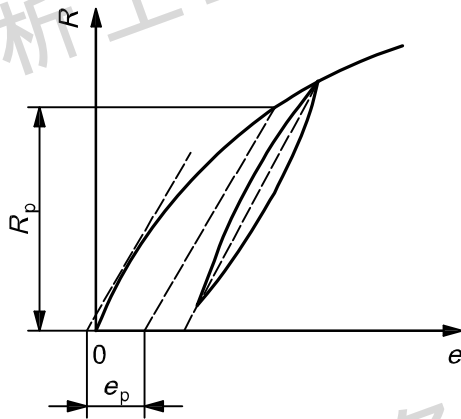
Figure 4 — Proof stress, total extension, R_t



Key

- e = elongation or extension
- e_r = elongation at peak force or extension
- R = force
- R_r = peak force

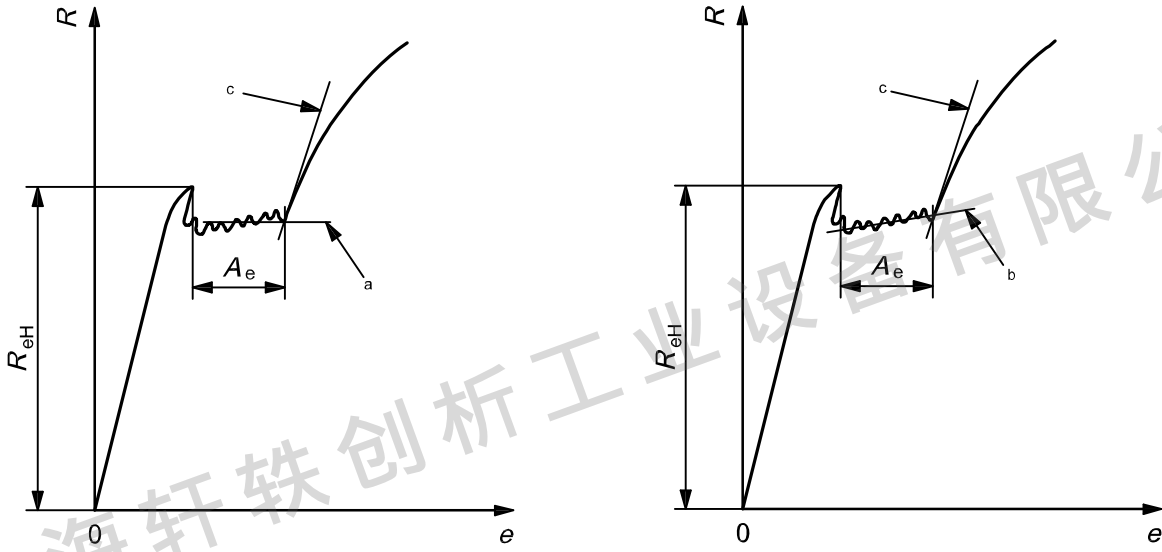
Figure 5 — Peak force, R_r



Key

- e = extension
- e_p = permanent extension
- R = force
- R_p = proof force, extension

Figure 6 — Proof force, extension, R_p , alternative procedure (see 13.1)



a) Horizontal method

b) Re method

Key

A_e area of yield point elongation

e strain

R stress

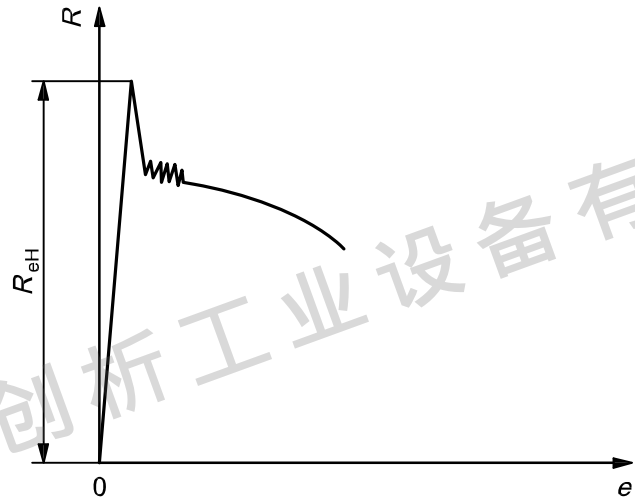
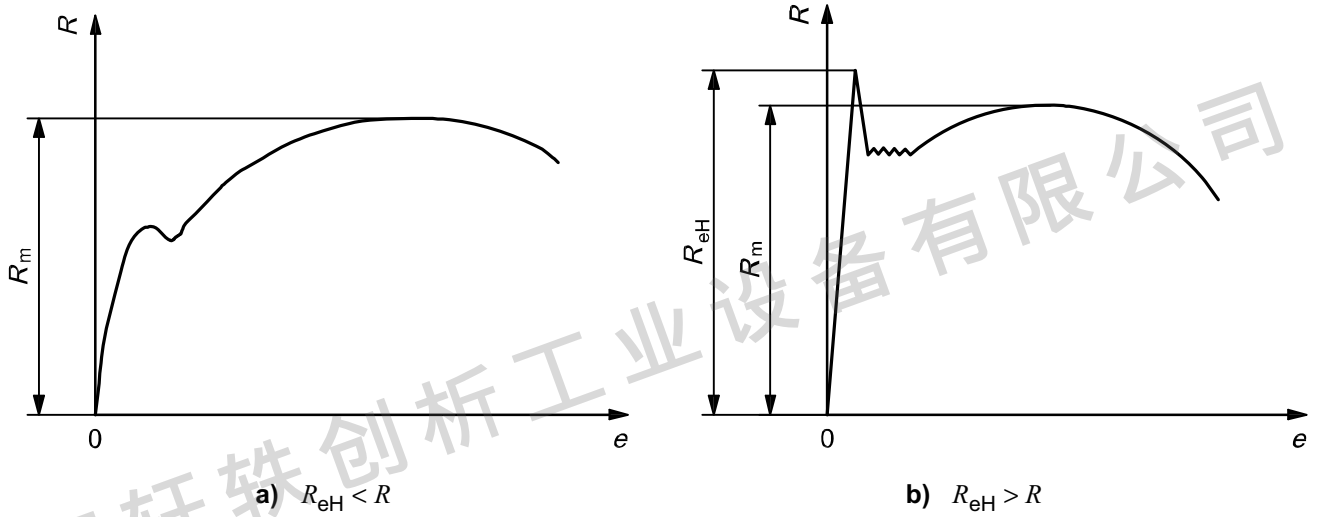
R_{eH} upper yield stress

a) Horizontal method: the distance between the vertical lines through the yield point and the end of the yield point elongation.

b) Re method: the distance between the vertical lines through the yield point and the end of the yield point elongation.

Le ore od tote et lo e o te urr atte tart o u or work arde .

Figure 7 — Determination of yield strength R_{eH} and A_e



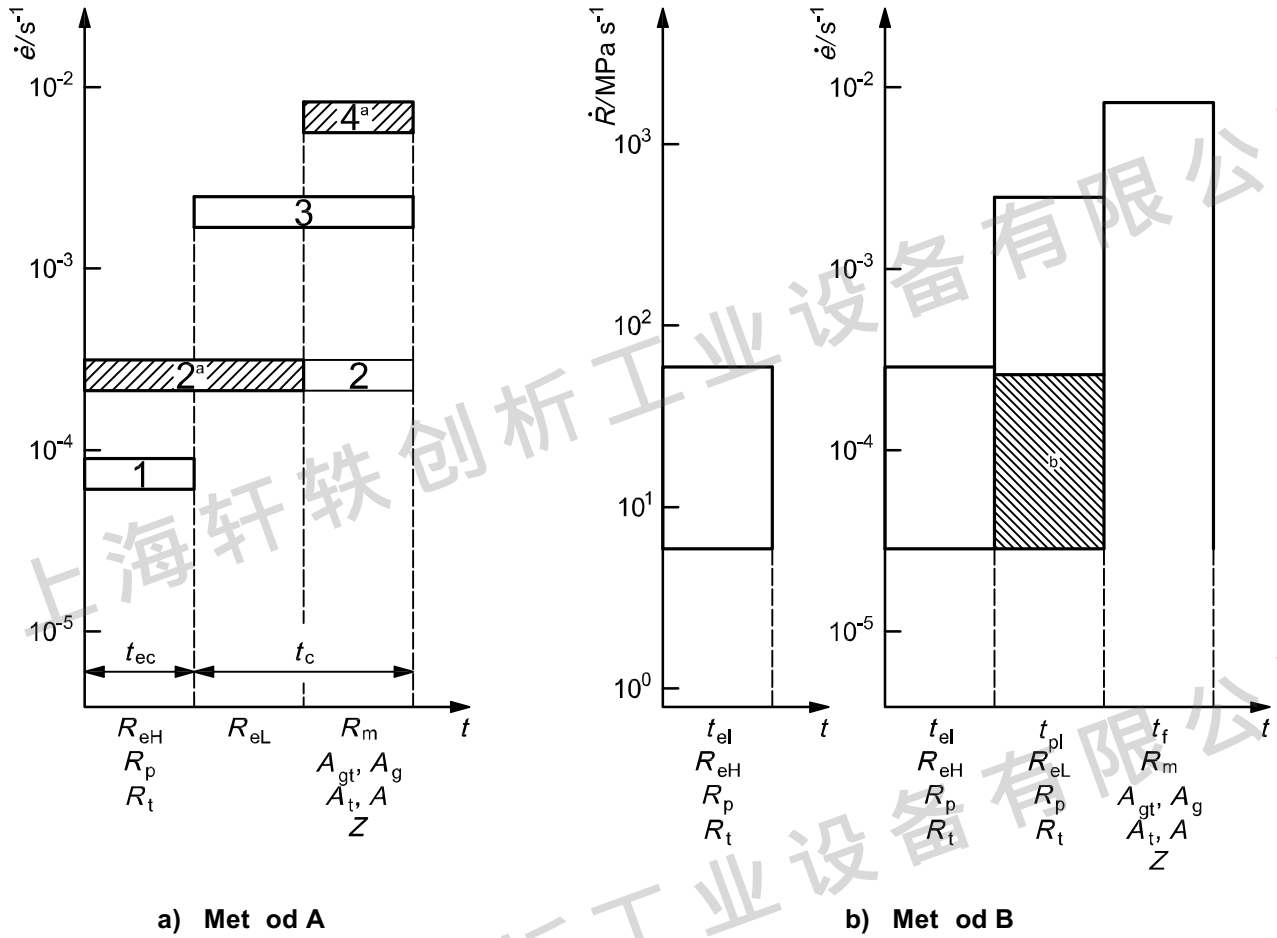
) S e al a e o tre - er e ta e exte o be av our^a

Key

- e er e ta e exte o
- R tre
- R_{eH} u er yield tre t
- R te le tre t

^a For ateral w id lay t be av our, o te le tre t de ed a ord to t art o SO 6892. e e ary, e arate a ree e t a be ade between te arte o er ed.

F ure 8 — D ere t ty e o tre -exte o urve or deter at o o te le tre t , R

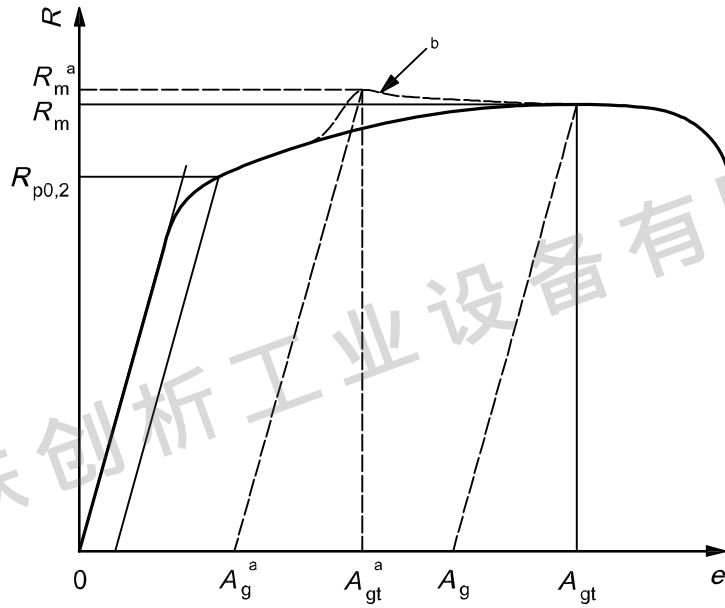


Key

- $\dot{\epsilon}$ strain rate
- \dot{R} stress rate
- t test duration
- t_e extended test duration
- t_{el} test duration (elastic behaviour) or determination of yield strength (see Table 1 or definition)
- t_{pl} test duration (usually ultimate) or determination of yield strength (see Table 1 or definition)
- t_f test duration (plastic behaviour) or determination of yield strength (see Table 1 or definition)
- 1 rate 1: $\dot{\epsilon} = 0,007 \text{ s}^{-1}$, with a relative tolerance of $\pm 2\%$
- 2 rate 2: $\dot{\epsilon} = 0,025 \text{ s}^{-1}$, with a relative tolerance of $\pm 2\%$
- 3 rate 3: $\dot{\epsilon} = 0,2 \text{ s}^{-1}$, with a relative tolerance of $\pm 2\%$
- 4 rate 4: $\dot{\epsilon} = 0,67 \text{ s}^{-1}$, with a relative tolerance of $\pm 2\%$ ($0,4 \text{ s}^{-1}$, with a relative tolerance of $\pm 2\%$)
- ^a Recommended.
- ^b Example of rate to lower rate, test at a rate of a higher or lower strain rate (see 1.4.2.5).

NOTE Strain rate to be used during the test is calculated from the stress rate using a Young's modulus of 210 GPa (steel).

Figure 9 — Illustration of strain rate to be used during the test, $R_{eH}, R_{eL}, R, R_t, R, A, A_t, A, A_t$ and are determined



Key

e — displacement

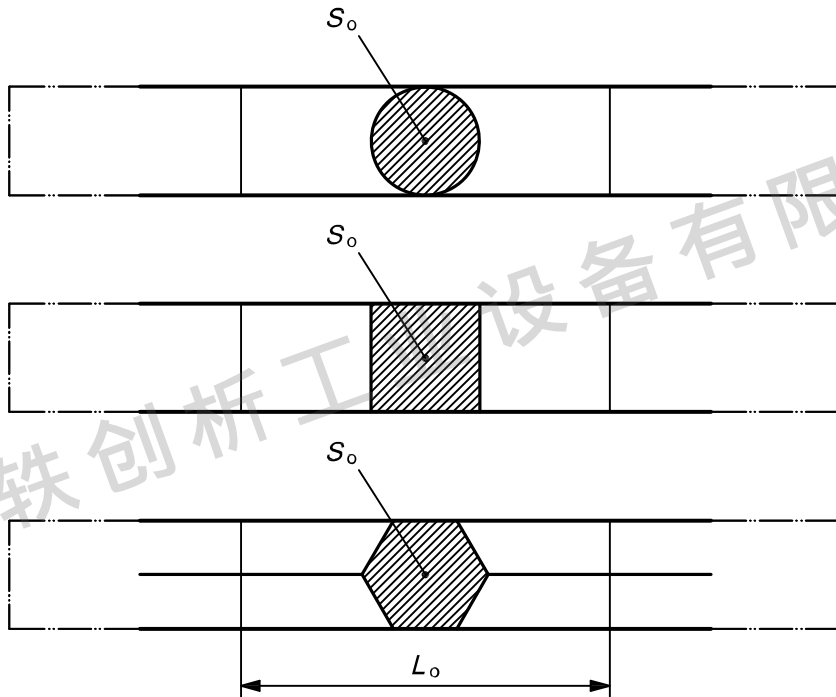
R — force

^a — Failure value, result from a abrupt rate test.

^b — Stress-strain behaviour, rate abruptly reduced.

NOTE For parameter details, see Table 1.

Figure 1 — Illustration of a standard duty test stress-strain curve

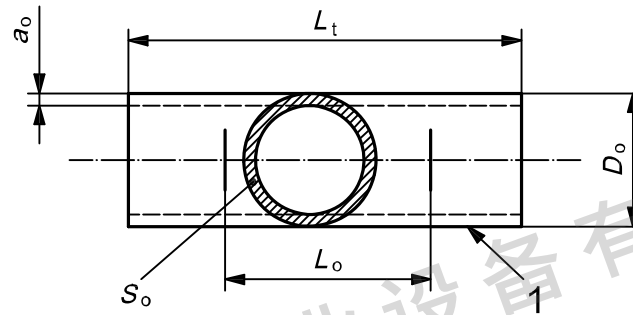


Key

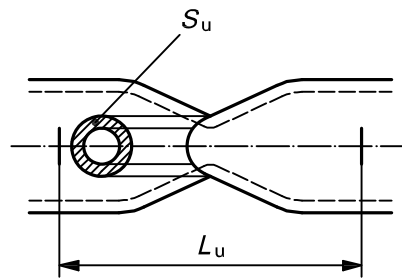
L_0 or total length

S_0 or total cross-sectional area

Figure 12—Test specimen area and length (see Annex C)



a) Before test

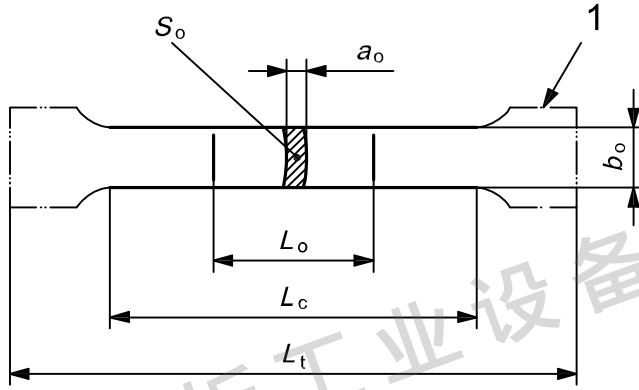


b) After test

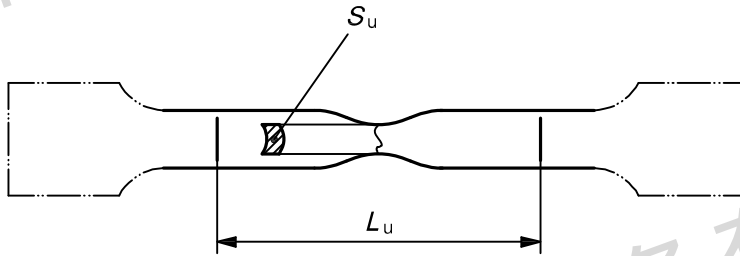
Key

- a_o or al wall t k e o a tube
- D_o or al exter al d a eter o a tube
- L_o or al au e le t
- L_t total le t o t e e e
- L_u al au e le t a ter ra ture
- S_o or al r o - e t o al area o t e arallel le t
- S_u u r o - e t o al area a ter ra ture
- 1 r e d e d

F ure 14 — Te t e e o r a le t o tube (ee A ex E)



a) Before test



b) After test

Key

- a_0 or al wall t k e o a tube
- b_0 or al avera e wd t o t e l o t u d al t r t a k e r o a tube
- L arallel le t
- L_0 or al au e le t
- L_t total le t o t e t e e
- L_u al au e le t a t e r r a t u r e
- S_0 or al r o - e t o al a r e a o t e arallel le t
- S_u u r o - e t o al a r e a a t e r r a t u r e
- 1 r e d e e d

NOTE T e a e o t e t e t - e e e a d o l y v e a a u d e.

F ure 15 — T e t e e u t r o a t u b e (e e A e x E)

A Annex A (Normative)

Requirements for user-controlled test data

A.1 General

This annex adds to the requirements for the determination of a material property by a user-controlled test data. Particular provisions for test data that could be taken into account for the test results.

The requirements are related to the test data, the software of the test data validation, and to the test results.

A.2 Terms and definitions

For the purpose of this annex, the following definitions apply.

A.2.1

User-controlled test data is data generated or controlled by the user, the test data, the test results, and the data records are undertaken by the user.

A.3 Test results

A.3.1 Data

The data could be defined in order to provide out of the value also used in the test results. The test results are not provided, the data user could be raw data with or without the raw data have been obtained and treated by the software. They could be used by the user. In the test results, the test results, the test results, the test results, the test results. An example of the test results is given in Figure A.1.

```

A {
    "Reference";"ISO 6892"
    "Identification";"TENSTAND"
    "Material";"DC 04 Steel"
    "Extensometer to crosshead transition";0.00;"%"
    "Specimen geometry";"Flat"
    "Specimen thickness = ao"
    "Specimen width = bo"
    "Cross-sectional area = So"
    "Extensometer gauge length = Le"
    "Extensometer output in mm"
    "Parallel length = Lc"
    "Data acquisition rate 50Hz"
    "Data row for start force reduction (Hysteresis) = Hs"
    "Data row for end force reduction (Hysteresis) = He"
    "Data row for switch to crosshead = Cs"
    "File length N data rows"
    "File width M data columns"
    .
    .
    .
B {
    "ao";0.711;"mm"
    "bo";19.93;"mm"
    "So";14.17;"mm2"
    "Le";80.00;"mm"
    "Lc";120.00;"mm"
    "N";2912
    "M";4
    "Hs";0
    "He";0
    "Cs";0
    .
    .
    .
C {
    "time";"crosshead";"extensometer";"force"
    "s";"mm";"mm";"kN"
    .
    .
    .
    0.40;0.0012;0.0000;0.12694
    0.42;0.0016;0.0000;0.12992
    0.44;0.0020;0.0001;0.13334
    0.46;0.0024;0.0002;0.13699
    0.48;0.0029;0.0003;0.14114
    0.50;0.0035;0.0004;0.14620
    0.52;0.0041;0.0006;0.15124
    0.54;0.0047;0.0007;0.15669
    0.56;0.0054;0.0008;0.16247
    0.58;0.0060;0.0009;0.16794
    0.60;0.0067;0.0012;0.17370
    0.62;0.0074;0.0013;0.17980
    0.64;0.0082;0.0014;0.18628
    .
    .
    .
    
```

Key

- A eader
- B te t ara eter a d a le d e o
- C data

Figure A.1 — Example of test data table

A.3.2 Data analysis

The requirements of the test method shall be applied to the data analysis. The requirements could be used to order the data to be used. For example to a true R_{eH} , Equation (A.1) may be used to determine the value of R_{eH} :

$$R_{eH} = \frac{\dot{\epsilon} E}{q} \times 1 \tag{A.1}$$

w ere

$\dot{\epsilon}$ the true rate, real or d ;

E the modulus of elasticity, real ;

R_{eH} the upper yield stress, real ;

q the relative or percentage error, expressed as a percentage of the test value (according to SO 75 -1).

The value of R_{eH} in Equation (A.1) due to the effect of the test rate should be used as the required value for the yield stress R_{eH} should be used as the required value for the yield stress.

Equation (A.2) should be used, the value of R_{eH} should be calculated using

$$= \frac{\dot{R}}{R_{eH} q} \times 1 \quad (A.2)$$

w ere \dot{R} the true rate, real or d.

A.4 Determination of the real rate

A.4.1 General

The following requirements should be taken into account by the software used.

A.4.2 Upper yield stress

R_{eH} (3.1.2.1) should be determined as the true stress corresponding to the value of the force or the reduction of at least 0.5% of the force, and followed by a reduction of the force of not exceeding the previous maximum over a strain rate of less than 0.5%.

A.4.3 Proportional limit stress and yield stress at total extension

R_p (3.1.3) and R_t (3.1.4) should be determined by the relation between the force and the extension.

A.4.4 Percentage total extension at maximum force

A_t (see 3.6.4 and Figure 1) should be determined as the total extension corresponding to the maximum force of the stress-strain curve at the yield point.

For the material to be tested the stress-strain curve with a maximum force should be determined. The maximum force should be determined. The maximum force should be determined. The maximum force should be determined.

A.4.5 Percentage total extension at maximum force

A (see 3.6.5 and Figure 1) should be determined as the total extension corresponding to the maximum force of the stress-strain curve at the yield point.

For the material to be tested the stress-strain curve with a maximum force should be determined. The maximum force should be determined. The maximum force should be determined.

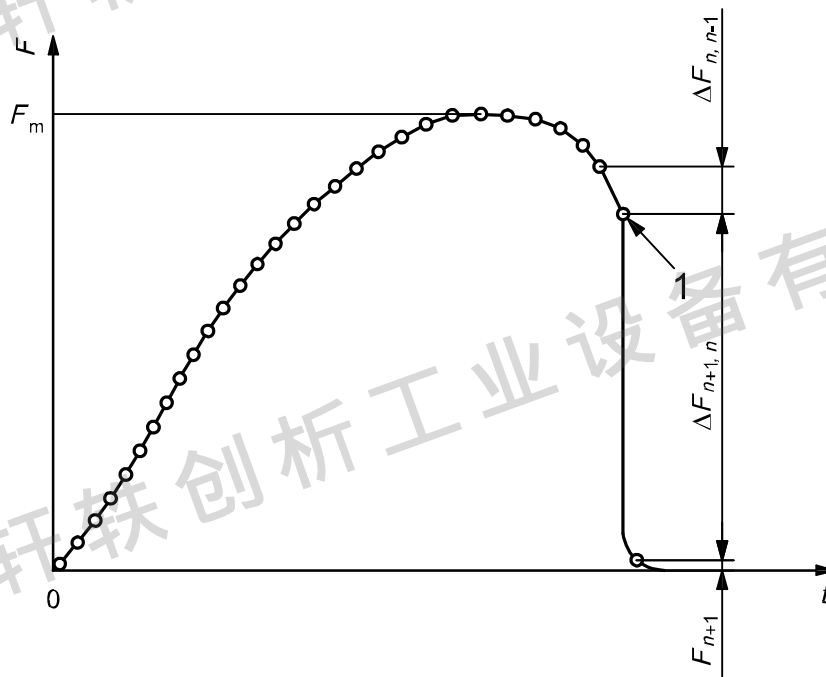
A.4.6 Performance at a temperature

A.4.6.1 Determine A_t with reference to the test temperature F using A.2.

The temperature is considered to be effective when the test is between two consecutive test results:

- a) by more than one test result between the value of the previous two test results, followed by a test result to lower than 2% of the maximum force;
- b) lower than 2% of the maximum force (optional).

Another useful method for detecting the temperature of the test is to monitor the voltage or electric current through the test piece, where the value measured will be more effective than the recorded data at a temperature.



Key

- F force
- F_{max} maximum force
- F_{+1} force at test result $+1$
- ΔF_{-1} difference between test result n and $n-1$
- ΔF_{+1} difference between test result $n+1$ and n
- t time
- 1 temperature
- data point

Criteria for a temperature

$$|\Delta F_{+1}| > 5|\Delta F_{-1}|$$

and/or

$$F_{+1} < 0.98 F_{max}$$

Figure A.2 — Sequence of test results to determine the test temperature

NOTE 1 The procedure for calculating the average lateral force for the test is as follows: the lateral force is divided by the area of the lateral surface of the specimen. The average lateral force is then multiplied by the area of the lateral surface of the specimen to give the average lateral force.

Other methods are used, e.g. the use of a re-determined data to allow lateral work to be normalized to a quality assurance level, etc. These methods would meet the requirements set out in Table A.1.

NOTE 2 A part of the EU-adopted TENSTAND report (GBRD-CT-2 - 412), ASC data file were produced with a reduced value of the lateral force that may be used or validated in software. Available (29-7-23) at <http://www.bsi.com/standards/tenstand>. Further details are given in Reference 21 and 22.

Table A.1 — Maximum permitted difference between outer-derived and usually derived results

Parameter	D^a		b	
	Relative	Absolute	Relative	Absolute
R_{2}	≤ 0,5 %	2 MPa	≤ 0,35 %	2 MPa
R_{1}	≤ 0,5 %	2 MPa	≤ 0,35 %	2 MPa
R_{eH}	≤ 1 %	4 MPa	≤ 0,35 %	2 MPa
R_{eL}	≤ 0,5 %	2 MPa	≤ 0,35 %	2 MPa
R	≤ 0,5 %	2 MPa	≤ 0,35 %	2 MPa
A	—	≤ 2 %	—	≤ 2 %

$$D^a = \frac{1}{n} \sum_{i=1}^n D_i$$

$$b = \sqrt{\frac{1}{n-1} \sum_{i=1}^n (D_i - D)^2}$$

where D_i is the difference between the result of a single evaluation, H_i , and the result of another evaluation, R_i , or a test error ($D_i = H_i - R_i$);

the number of test results is n ($n \geq 5$).

The relative and absolute values could be taken to account.

A ex B (or atve)

**Typ e o te t e e to be u ed or t rodu t : eet , tr a d lat
betwee ,1 a d 3 t k**

NOTE For rodu t o le t a ,5 t k e , e al re auto ay be e e ary.

B.1 S a e o t e t e e

Ge erally, t e t e e a r ed e d w are w der t a t e arallel le t . T e arallel le t , L , all be o e ted to t e e d by ea o tra to urve wt a radu o at lea t 2 . T e w dt o t e e e d ould be $\geq 1,2b_0$, w ere b_0 t e or al w dt .

By a ree e t, t e t e e ay al o o to a tr wt arallel de (arallel ded te t e e). For rodu t o w dt equal to or le t a 2 , t e w dt o t e t e e ay be t e a e a t a t o t e rodu t .

B.2 D e o o t e t e e

T ree d ere t o - ro ort o al te t e e eo etre are wdely u ed (ee Table B.1).

T e arallel le t all ot be le t a $L_0 + b_0/2$.

a e o d ute, t e le t $L_0 + 2b_0$ ould be u ed, u le t ere u e t ateral.

For arallel de t e e le t a 2 w de, a d u le ot erw e e e d t e rodu t ta dard, t e or al au e le t , L_0 , all be equal to 5 . For t ty e o te t e e, t e ree le t betwee t e r all be equal to $L_0 + 3b_0$.

W e ea ur t e d e o o ea te t e e, t e to lera e o a e ve Table B.2 all a ly.

For te t e e w ere t e w dt t e a e a t a t o t e rodu t, t e or al ro - e to al area, S_0 , all be al ulated o t e ba o t e ea ured d e o o t e t e e.

T e o al w dt o t e t e e ay be u ed, rov ded t a t e a to lera e a d to lera e o a e ve Table B.2 ave bee o led wt , to avo d ea ur t e w dt o t e t e e a t t e e o t e t e t .

Table B.1 — D e o o t e t e e

D e o l l e t r e

T e t e e t y e	W d t b_0	O r a l a u e l e t L_0	P a r a l l e l e t		F r e e l e t b e t w e e t e r o r a r a l l e d e d t e t e e
			M u	R e o e d e d	
1	12,5 ± 1	5	57	75	87,5
2	2 ± 1	8	9	12	14
3	25 ± 1	5 ^a	6 ^a	—	Not de ed

^a T e r a t o L_0/b_0 a d L/b_0 o a t y e 3 t e t e e o a r o t o e o t y e 1 a d 2 v e r y l o w . A a r e u l t t e r o e r t e , e e e l l y t e e l o a t o a t e r r a t u r e (a b s o l u t e v a l u e a d a t t e r r a t e) , e a u r e d w t t t e t e e w i l l b e d e r e t r o t e o t e r t e t e e t y e .

Table B.2 — T o l e r a e o t e w d t o t e t e t e e

D e o a d t o l e r a e l l e t r e

N o a l w d t o t e t e t e e	M a t o l e r a e ^a	T o l e r a e o a e ^b
12,5	± , 5	, 6
2	± , 1	, 12
25	± , 1	, 12

^a T e e t o l e r a e a r e a l a b l e t e o a l v a l u e o t e o r a l r o - e t o a l a r e a , S_0 , t o b e l u d e d t e a l u l a t o w t o u t a v t o e a u r e t .

^b M a x u d e v a t o b e t w e e t e e a u r e e t o t e w d t a l o t e e t r e a r a l l e l e t , L , o t e t e t e e .

B.3 P r e a r a t o o t e t e e

T e t e t e e a l l b e r e a r e d o a o t t o a e t t e r o e r t e o t e a l e . A y a r e a w a v e b e e a r d e d b y e a r o r r e a l l b e r e o v e d b y a .

T e e t e t e e a r e r e d o a t l y r e a r e d r o e e t o r t r . o b l e , t e a - r o l l e d u r a e o u l d o t b e r e o v e d .

NOTE T e r e a r a t o o t e e t e t e e b y u a r e u l t a t a e t o t e a t e r a l r o e r t e , e e e l l y t e y e l d / r o o t r e t (d u e t o w o r k a r d e) . M a t e r i a l w e x b t w o r k a r d e o u l d , e e r a l l y , b e r e a r e d b y l l , r d e t .

F o r v e r y t a t e r a l , t r e o e d e d t a t t r o d e t a l w d t o u l d b e u t a d a e b l e d t o a b u d l e w t t e r e d a t e l a y e r o a a e r w r e t a t t o t e u t t o l . E a a l l b u d l e o t r o u l d t e b e a e b l e d w t a t k e r t r o e a d e , b e o r e a t o t e a l d e o o t e t e t e e .

T e t o l e r a e v e T a b l e B.2, e . ± , 5 o r a o a l w d t o 12,5 , e a t a t o t e t e e a l l a v e a w d t o u t d e t e t w o v a l u e v e b e l o w , t e o a l v a l u e o t e o r a l r o - e t o a l a r e a , S_0 , t o b e l u d e d t e a l u l a t o w t o u t a v t o e a u r e t :

$$12,5 + , 5 = 12,55$$

$$12,5 - , 5 = 12,45$$

B.4 Determination of theoretical area

S_0 shall be calculated from the area measured to the nearest 0.01 mm².

The error in the theoretical area shall not exceed $\pm 2\%$. At the least, the error in the area measured to the nearest 0.01 mm² shall not exceed $\pm 0.2\%$.

In order to achieve the result with a reduced area uncertainty, the theoretical area shall be determined with an accuracy of $\pm 1\%$ or better. For the lateral area, the uncertainty may be reduced.

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A ex C (or atve)

Ty e o te t e e to be u ed or wre, bar a d e to wt a d a eter or t k e o le t a 4

C.1 S a e o t e t e e

T e t e t e e e e rally o t o a u a e d or to o t e rodu t (ee F ure 12).

C.2 D e o o t e t e e

T e or al au e le t , L_0 , all be take a 2 ± 2 , or 1 ± 1 . T e d ta e betwee t e r o t e a e all be equal to at lea t $L_0 + 3b_0$ but a u o $L_0 + 2$.

t e e r e t a e lo a t o a t e r a t u r e o t to be deter e d, a d ta e betwee t e r o at lea t 5 ay be u ed.

C.3 Pre arat o o te t e e

t e rodu t delvered o led, are all be take t r a t e t .

C.4 Deter at o o t e or al ro - e t o al area

Deter e S_0 to a a u r a y o $\pm 1\%$ or better.

For rodu t o r ular ro - e t o , t e or al ro - e t o al area ay be al ulated ro t e art et ea o two ea ure e t arred out two e r e d ular d r e t o .

T e or al ro - e t o al area, S_0 , quare ll etre , ay be deter e d ro t e a o a k ow le t a d t d e t y u Equato (C.1):

$$S_0 = \frac{1}{\rho L_t} \tag{C.1}$$

w ere

t e a , r a , o t e t e t e e;

L_t t e total le t , ll etre , o t e t e t e e;

ρ t e d e t y , r a e r u b e t etre, o t e t e t e e a t e r a l.

A ex D (or atve)

Type o te t e e to be u ed or eet a d lat o t k e equal to
or reater t a 3 , a d w re, bar a d e to o d a eter or
t k e equal to or reater t a 4

D.1 S a e o t e t e e

U ually, t e t e e a e d a d t e arallel le t all be o e ted by ea o tra to rad to
t e r e d e d w ay be o a y u table a e o t e r o t e t e a e (ee F ure 13). T e
u tra to rad u betwe t e r e d e d a d t e arallel le t all be:

- a) $,75d_0$, w ere d_0 t e d a eter o t e arallel le t , or t e yl dr al t e t e e ;
- b) 12 or o t e r t e t e e .

Se to , bar , et ., ay be te ted u a ed, required.

T e ro - e to o t e t e t e e ay be r ular, quare, re ta ular or, e al a e , o a o t e r a e.

For t e t e e w t a re ta ular ro - e to , t re o e ded t a t t e w d t o t k e r a t o ould o t
ex eed 8:1.

e eral, t e d a eter o t e arallel le t o a e d yl dr al t e t e e all be o t le t a 3 .

D.2 D e o o t e t e t e e

D.2.1 Parallel le t o a e d t e t e e

T e arallel le t , L , all be at lea t equal to:

- a) $L_0 + (d_0/2)$ or yl dr al t e t e e ;
- b) $L_0 + 1,5\sqrt{S_0}$ or o t e r t e t e e .

a e o d ute, t e le t $L_0 + 2d_0$ or $L_0 + 2\sqrt{S_0}$ all be u ed de e d o t e t e o t e t e e,
u le t e r e u e t a t e r a l.

D.2.2 Le t o u a e d t e t e e

T e r e e le t betwe t e r o t e a e all be adequate or t e au e ark to be at lea t a
d t a e o $\sqrt{S_0}$ r o t e r .

D.2.3 Or al au e le t

D.2.3.1 Pro ort o al te t e e

A a e eral rule, ro ort o al te t e e are u ed w ere L_o related to t e or al ro - e to al area, S_o , by Equat o (D.1):

$$L_o = k\sqrt{S_o} \quad (D.1)$$

w ere k equal to 5,65.

Alter at vely 11,3 ay be u ed a t e k value.

Te t e e o r ular ro - e to ould reerably ave o e eto d e o ve Table D.1.

Table D.1 — C r ular ro - e to te t e e

Coe e to ro ort o al ty k	Da eter d	Or al au e le t $L_o = k\sqrt{S_o}$	M u arallel le t L
5,65	2	1	11
	14	7	77
	1	5	55
	5	25	28

D.2.3.2 No - ro ort o al te t e e

No - ro ort o al te t e e ay be u ed e ed by t e rodu t ta dard.

T e arallel le t, L , ould ot be le t a $L_o + b_o/2$. a e o d ute, t e arallel le t $L = L_o + 2b_o$ all be u ed u le t ere u e t ateral.

Table D.2 ve deta l o o e ty al te t e e d e o .

Table D.2 — Ty al lat te t e e d e o

W dt b_o	Or al au e le t L_o	M u arallel le t L	A rox ately total le t L_t
4	2	22	45
25	2	215	45
2	8	9	3

D.3 Pre arat o o te t e e

D.3.1 Ge eral

T e tolera e o t e tra ver ed e o o a ed te t e e are ve Table D.3.

A exa le o t e a l ato o t e e tolera e ve D.3.2 a d D.3.3.

D.4 Determination of the total area

The total area to be used to calculate S_0 or the effective regular or irregular or the total area of all our data at any tolerance level Table D.3. For all other areas of the total area, the total area will be calculated to ensure that the error rate does not exceed $\pm 0.5\%$ of the total area.

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A ex E
(or atve)

Ty e o t e t e e t o b e u e d o r t u b e

E.1 S a e o t e t e t e e

T e t e t e e o t e t e r o a l e t o t u b e , o r a l o t u d a l o r t r a v e r e t r u t r o t e t u b e a d a v t e u l t k e o t e w a l l t u b e (s e e F i g u r e 1 4 a d 1 5) , o r o a t e t e e o r u l a r r o - e t o a e d r o t e w a l l o t e t u b e .

M a e d t r a v e r e , l o t u d a l a d r u l a r r o - e t o t e t e e a r e d e r i b e d A e x B o r t u b e w a l l t k e l e t a 3 , a d A e x D o r t k e e q u a l t o o r r e a t e r t a 3 . T e l o t u d a l t r e e r a l l y u e d o r t u b e w t a w a l l t k e o r e t a , 5 .

E.2 D e o o t e t e t e e

E.2.1 L e t o t u b e

T e t u b e l e t t a y b e l u e d a t b o t e d . T e r e e l e t b e t w e e e a l u a d t e e a r e t a u e a r k a l l b e r e a t e r t a $D_o/4$. a e o d u t e , t e v a l u e , D_o , a l l b e u e d , t e r e u e t a t e r a l .

T e l e t o t e l u r o e t b e y o d t e r o t e a e t e d r e t o o t e a u e a r k a l l o t e x e e d D_o , a d t a e a l l b e u t a t d o e o t t e r e r e w t d e o r a t o o t e a u e l e t .

E.2.2 L o t u d a l o r t r a v e r e t r

T e a r a l l e l e t , L , o t e l o t u d a l t r a l l o t b e l a t t e d b u t t e e a d a y b e l a t t e d o r r t e t e t a e .

T r a v e r e o r l o t u d a l t e t e e d e o o t e r t a t o e v e A e x e B a d D a b e e e d t e r o d u t t a d a r d .

S e a l r e a u t o a l l b e t a k e w e t r a t e t e t r a v e r e t e t e e .

E.2.3 C r u l a r r o - e t o t e t e e a e d t u b e w a l l

T e a l o t e t e t e e e e d t e r o d u t t a d a r d .

E.3 D e t e r a t o o t e o r a l r o - e t o a l a r e a

S_o o r t e t e t e e a l l b e d e t e r e d t o t e e a r e $\pm 1\%$ o r b e t t e r .

T e o r a l r o - e t o a l a r e a , S_o , q u a r e l l e t r e , o t e l e t o t u b e o r l o t u d a l o r t r a v e r e t r a y b e d e t e r e d r o t e a o t e t e t e e , t e l e t o w a b e e a u e d , a d r o t d e t y u E q u a t o (E . 1) :

$$S_o = \frac{1}{\rho L_t} \tag{E.1}$$

where

t_e is the thickness of the tube wall;

L_t is the total length of the tube;

ρ is the density of the material.

The theoretical area, S_o , of the tube is calculated according to Equation (E.2):

$$S_o = \frac{b_o}{4}(D_o^2 - b_o^2)^{1/2} + \frac{D_o^2}{4} \arcsin \left(\frac{b_o}{D_o} \right) - \frac{b_o}{4} \left[\left(\frac{D_o^2 - b_o^2}{4} \right)^{1/2} - \left(\frac{D_o^2 - b_o^2}{4} \right)^{1/2} \right] \quad (E.2)$$

where

a_o is the thickness of the tube wall;

b_o is the average width of the tube;

D_o is the external diameter of the tube.

The theoretical area, S_o , can be used for the following conditions:

$$\left. \begin{aligned} S_o &= a_o b_o \left[\frac{b_o}{D_o} < 0,25 \right] \\ S_o &= a_o b_o \left[\frac{b_o}{D_o} < 0,1 \right] \end{aligned} \right\} \quad (E.3)$$

For the tube, the theoretical area, S_o , is calculated according to Equation (E.4):

$$S_o = \pi a_o (D_o - a_o) \quad (E.4)$$

A ex F
(or atve)

**E t ato o t e r o ead e arato rate o derato o
t e t e (or o la e) o t e t e t a e**

Equato (1) doe ot o der a yela t de or ato o t e t e t equ e t (ra e, load ell, r , et .).
T e a t t e de or ato a be e arated to t e e la t de or ato o t e t e t equ e t a d
t e de or ato o t e t e t e e. O ly a ar o t e r o ead e arato rate tra erred to t e t e t e e.
T e re ult tra rate at t e t e t e e, \dot{e} , re r o al e o d , ve by Equato (F.1) (ee
Re ere e 39):

$$\dot{e} = v / \left(\right) \tag{F.1}$$

w ere

C_M t e t e , ewto er ll etre, o t e t e t equ e t (arou d t e o t o t e r e t u
a $R_{,2}$, t e ot l ear, e. .w e u wed e r);

L t e arallele t , ll etre , o t e t e t e e;

t e lo e, e a a al, o t e t e - e r e t a e exte o urve a t a ve o e t o t e t e t
(e. .arou d t e o t o t e r e t u a $R_{,2}$);

S_o t e or al ro - e t o area, quare ll etre ;

v t e r o ead e arato rate, ll etre er e o d.

NOTE T e value o a d C_M derved ro t e l ear orto o t e t e / tra urve a ot be u ed.

Equato (1) doe ot o e ate or t e e e t o o la e (ee 1 .3.1). A better a rox ato o t e
ro ead e arato rate, v , ll etre er e o d, e e ary to rodu e a re ult tra rate at t e
t e t e e, \dot{e} , arou d t e o t o t e r e t , a be ade ro Equato (F.2) (ee Re ere e 4):

$$v = \dot{e} \left(\right) \tag{F.2}$$

A ex G
(or atve)

**Mea ur t e er e ta e elo ato a ter ra ture t e e ed value
le t a 5%**

Pre auto ould be take w e ea ur t e er e ta e elo ato a ter ra ture t e e ed value
le t a 5%.

O e o t e r e o e ded et od a ollow .

Pr or to t e t e t a very all ark ould be ade lo e to ea e do t e arallel le t . U a a r o
eedle- o ted d v der et at t e au e le t , a ar r bed wt t e ark a a e tre. A ter ra ture, t e
broke t e t e e ould be la ed a xt ure a d ax al o re ve o r ea led, re erably by ea o a
rew, u e t to r ly old t e e e to et er dur ea ure e t. A e o d a r o t e a e radu
ould t e be r bed ro t e or al e tre lo e t to ra ture, a d t e d ta e betwee t e two rat e
ea ured by ea o a ea ur ro o e or ot er utable tru e t. or der to re der t e e
rat e ore ea ly v ble, a utable dye l ay be a led to t e t e e be ore t e t .

NOTE A ot er et od de r bed 2 .2 (ea ur exte o at ra ture u a exte o eter).

A ex H (or atve)

Mea ure e t o er e ta e elo ato a ter ra ture ba ed o ubd v o o t e or al au e le t

To avo d av to ree tte t e e w er e t e o to o t e ra ture doe ot o ly wt t e o d to o 2 .1, t e ollow et o d ay be u e d, by a ree e t:

- a) be ore t e t, ubd v de t e or al au e le t , L_o , to N equal le t o 5 (re o e ded) to 1 ;
- b) a ter t e t, u e t e y bo l X to de o t e t e au e ark o t e or ter ar to t e t e e a d t e y bo l Y or t e au e ark o t e lo er ar to t e t e e w at e a e d ta e ro t e ra ture a ark X .

t e u ber o terval betwee X a d Y , t e elo ato a ter ra ture dete r e d a ollow :

- 1) N - a eve u ber ee F ure H.1 a), ea ure t e d ta e betwee X a d Y , l_{XY} , a d t e d ta e ro Y to t e raduat o ark , l_Y , lo ated at $(N-)/2$ terval beyo d Y .

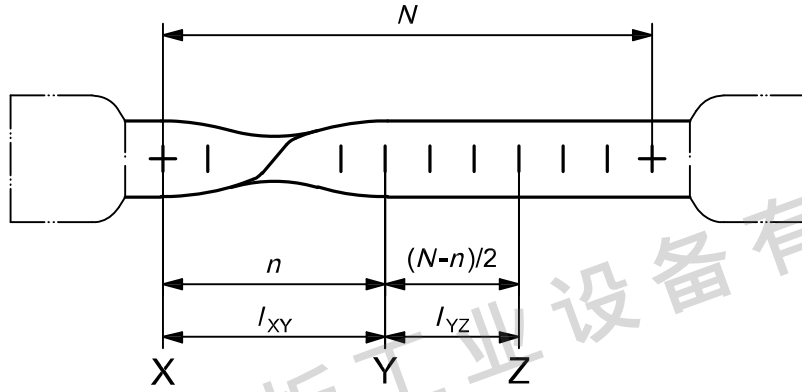
Cal ulate t e er e ta e elo ato a ter ra ture, A , u Equato (H.1):

$$A = \frac{l_{XY} + 2l_Y - L_o}{L_o} \times 1 \quad (H.1)$$

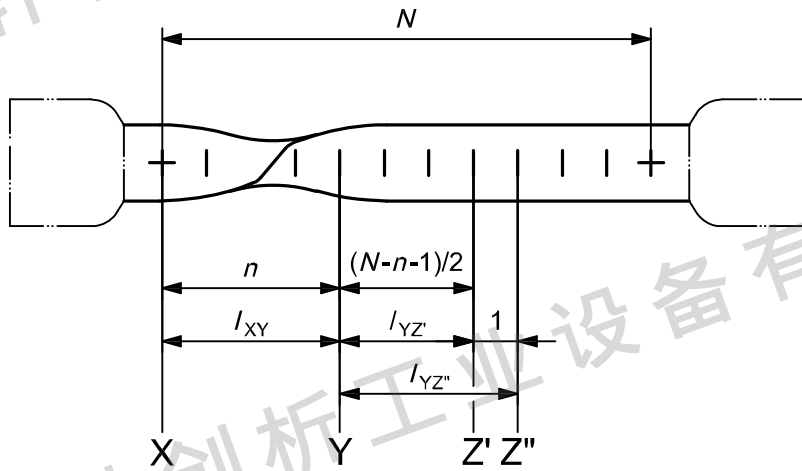
- 2) N - a odd u ber ee F ure H.1 b), ea ure t e d ta e betwee X a d Y a d t e d ta e ro Y to t e raduat o ark ' a d ", l_Y , a d l_Y ", lo ated re e tvely at $(N- - 1)/2$ a d $(N- + 1)/2$ terval beyo d Y .

Cal ulate t e er e ta e elo ato a ter ra ture u t e equato :

$$A = \frac{l_{XY} + l_Y ' + l_Y '' - L_o}{L_o} \times 1 \quad (H.2)$$



a) N – a even u ber



b) N – a odd u ber

Key

- n u ber o terval betwee X a d Y
- N u ber o equal le t
- X au e arko t e orter art o t e t e t e e
- Y au e arko t e lo er art o t e t e t e e
- , ' , " au e ark

NOTE Te a e o t e t e t e e e e ad o ly ve a a u de.

Figure H.1 — Exa le o ea ure e to er e ta e lo ato a ter ra ture

A ex
(or atve)

**Deter at o o t e er e ta e la t elo at o wt out e k , A_w ,
or lo rodu t u a bar , wre a d rod**

T et od to be er or ed o t e lo er ar to a broke te le te t e e.

Be ore t e t e t, equ d ta t ark are ade o t e au e le t, t e d ta e betwee two u e ve ark be equal to a ra o t e t al au e le t, L'_o . T e ark o t e t al au e le t, L'_u , ould be a urate to wt $\pm ,5$. T e ea ure e t o t e al au e le t a t e r ra ture, L'_u , ade o t e lo e t broke ar to t e t e e a d ould be a urate to wt $\pm ,5$.

order or t e ea ure e t to be val d, t e ollow two o d to ould be et:

- a) t e l t o t e ea ur zo e ould be lo ated at lea t $5d_o$ ro t e ra ture a d at lea t $2,5d_o$ t e r ;
- b) t e ea ur au e le t ould be at lea t equal to t e value e ed t e rodu t ta dard.

T e er e ta e la t elo at o wt out e k al ulated by Equat o (.1):

$$A_w = \frac{L'_u - L'_o}{L'_o} \times 1 \quad (.1)$$

NOTE For a y etall ateral t e ax u or e o ur t e ra ew ere e k tart . T ea t a t e value or A a d A_w or t e e ateral will be e arly equal. Lar e d ere e will be ou d ly old de or ed ateral u a double redu ed t late or rrad ated tru tural teel or te t er or ed at elevated te erature .

A ex J (or atve)

E t ato o t e u erta ty o ea ure e t

J.1 trodu to

The ex ve u da e o ow to e t ate t e u erta ty o t e value deter ed a orda e wt t art o SO 6892. t ould be oted t at t ot o ble to ve a ab olute tate e t o u erta ty or t te t et od be au e t ere are bot *ateral de e de t a d ateral de e de t* o t rbut o t o t e u erta ty tate e t. SO/EC Gu de 98-3⁴ a o re e ve do u e t o over 9 a e ba ed u o r orou tat t al et od or t e u ato o u erta te ro varou our e. t o lex ty a rovd t e drv or e or a u ber o or a zato to rodu e l ed ver o (ee NS 8¹⁵, NS 3³¹⁶, Re ere e 23). Tee do u e t all ve u da e o ow to e t ate u erta ty o ea ure e t ba ed u o a “u erta ty bud et” o e t. For detaled de r to , ee EN 1 291¹¹ a d Re ere e 24. Add to al or ato o t e e t ato o u erta ty avale Re ere e 25 a d 26. Te ea ure e t u erta ty re e ted ere doe ot de r bet e atter re ult ro t e o o e ty o t e ateral, e. . ro o e bat , ro t e be a d at tee do a extruded ro le or a rolled ol, or o d ere t o to wt a a t . Te u erta ty re ult ro t e atter o t e data obta ed ro d ere t t e t, d ere t a e, or d ere t lab take ro a deal o o e eou ateral. t e ollow , t e d ere t lue e are de r bed a d u da e or t e deter ato o t e u erta te ve .

NOTE Te re rodu bly value u ed Table J.2 to J.4 are al wdt terval a orda e wt SO/EC Gu de 98-3⁴ a d ould be ter reted a t e value o lu a d u (\pm) atter tolera e .

J.2 E t ato o u erta ty

J.2.1 Ge eral

The ta dard u erta ty, u , o t e value o a ara eter a be e t ated two way .

J.2.2 Ty e A — By re eated ea ure e t

$$u = \frac{s}{\sqrt{n}} \tag{J.1}$$

w ere

t e ta dard dev ato o t e ea ure e t ;

t e u ber o ob ervato be a vera ed to re ort t e re ult o t e ea ure e t u der or al ru ta e .

J.2.3 Ty e B — Fro o e ot er our e, e. . al brat o ert ate or tolera e

Here t e true value equally lkely to o ur a yw ere wt t e de ed terval o t e d t rbut o de r bed a re ta ular or u or . Here t e ta dard u erta ty ve by Equato (J.2):

$$u = \frac{a}{\sqrt{3}} \tag{J.2}$$

w ere a al t e wdt o t e terval w t e qua t ty a u ed to le.

O te t e e t a t o o a q u a t t y , y , v o l v e t e e a u r e e t o o t e r q u a t t e . T e e t a t o o t e u e r t a t y y a l l t a k e a o u t o t e o t r b u t o o t e u e r t a t e a l l t e e e a u r e e t . t t u k o w a a o b e d u e r t a t y . t e e t a t o l y v o l v e t e a d d t o o r u b t r a t o o a e r e o e a u r e e t , x₁, x₂ ... x , t e t e o b e d u e r t a t y y , u (y) , v e b y E q u a t o (J . 3) :

$$u(y) = \sqrt{u(x_1)^2 + u(x_2)^2 + \dots + u(x)^2} \tag{J.3}$$

w e r e u (x₁) t e u e r t a t y t e a r a e t e r x₁ , e t .

t e e t a t o o u (y) v o l v e u l t i a t o o t e r q u a t t e , t e t o t e e a e r t o w o r k w i t r e l a t v e t e r a l u l a t e d a e r e t a e o r o o e t v a l u e a d u e r t a t y .

J.3 Equ e t a r a e t e r e e t o t e u e r t a t y o t e t r e u l t

T e u e r t a t y o t e r e u l t d e t e r e d r o a t e l e t e t o t a o o e t d u e t o t e e q u e t u e d . a r o u t e t r e u l t a v e d e r u e r t a t y o t r b u t o d e e d o t e w a y t e y a r e d e t e r e d . T a b l e J . 1 d a t e t e e q u e t u e r t a t y o t r b u t o t a t o u l d b e o d e r e d o r o e o t e o r e o o a t e r a l r o r t e d e t e r e d a t e l e t e t . S o e o t e t e t r e u l t a b e d e t e r e d w i t a l o w e r u e r t a t y t a o t e r , e . . t e u e r y e l d t r e t , R_{eH} , o l y d e e d e t o t e u e r t a t e o e a u r e e t o o r e a d r o - e t o a l a r e a , w i t r o o t r e t , R , d e e d e t o o r e , e x t e o , a u e l e t a d r o - e t o a l a r e a . F o r r e d u t o o a r e a , t e e a u r e e t u e r t a t e o r o - e t o a l a r e a b o t b e o r e a d a t e r r a t u r e e e d t o b e o d e r e d .

Table J.1 — U e r t a t y o t r b u t o r t o t e t e t r e u l t

Para e t e r	T e t r e u l t					
	R _{eH}	R _{eL}	R	R	A	
For e	×	×	×	×	—	—
Exte o	—	—	—	×	×	—
Gau e l e t	—	—	—	×	×	—
S _o	×	×	×	×	—	×
S _u	—	—	—	—	—	×

NOTE
 × r e l e v a t
 — o t r e l e v a t

T e u e r t a t y o t e t e t r e u l t l i t e d T a b l e J . 1 a y b e d e r v e d r o t e a l b r a t o e r t a t e o t e d e v e u e d o r t e d e t e r a t o o t e t e t r e u l t . F o r e x a l e , t e t a d a r d u e r t a t y v a l u e o r a o r e a r a e t e r u a a e w t a e r t e d u e r t a t y o 1 , 4 % , w o u l d b e 1 , 4 / 2 o r , 7 % . t o u l d b e o t e d t a t a C l a 1 , l a a t o (o r t e t e l e t e t a e o r e x t e o e t e r) d o e o t e e e a r l y u a r a t e e a u e r t a t y o 1 % . T e u e r t a t y o u l d b e a t l y e r o r l o w e r (o r o r e e x a l e , e e S O 7 5 - 1) , a d t e e q u e t e r t a t e o u l d b e o u l t e d . U e r t a t y o t r b u t o d u e t o a t o r u a d r t o t e e q u e t e t a l b r a t o a d t u e d e r e t e v r o e t a l o d t o o u l d a l o b e t a k e t o a o u t .

C o t u t e e x a l e a o r d t o E q u a t o (J . 3) , t a k a o u t o t e u e r t a t e o r e o r e x t e o e t e r e a u r e e t , t e o b e d u e r t a t y o t e t e t r e u l t o r R_{eH} , R_{eL} , R a d A
 $\sqrt{(1,4/2)^2 + (1/\sqrt{3})^2} = \sqrt{,7^2 + ,58^2} = ,91%$, u t e q u a r e r o o t o t e u o t e q u a r e a r o a .

W e e t a t t e u e r t a t y o R , t o t a r o r a t e t o l y a l y t e u a t o o t e t a d a r d u e r t a t y o o e t r o t e l a a t o o t e e a u r d e v e . T e o r e - e x t e o u r v e a l l b e e x a e d . F o r e x a l e , t e d e t e r a t o o R o u r o t e o r e - e x t e o u r v e a t a o t o t e u r v e

A ex K
(or atve)

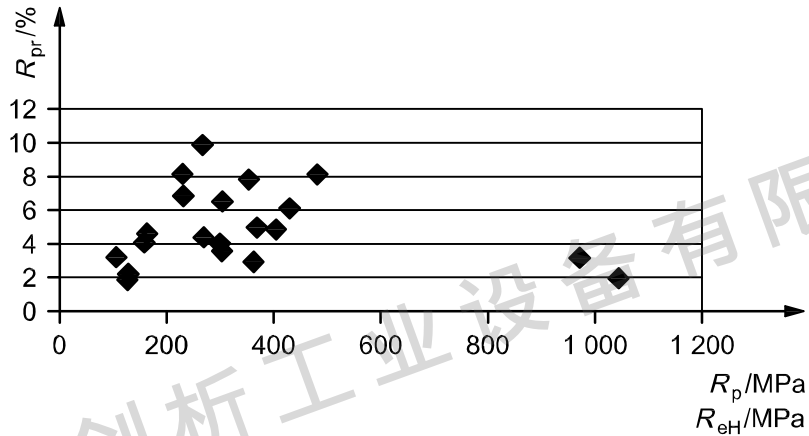
Pre o o te le te t — Re ult ro terlaboratory ro ra e

K.1 terlaboratory atter

A d ato o te ty al atter te le te t re ult or a variety o ateral t at ave bee re orted dur laboratory ter o ar o exer e , w lude bot ateral atter a d ea ure e t u erta ty, are ow Table K.1 to K.4. T e re ult or t e ro du b l ty are ex re e d a er e ta e al ulated by ult ly by 2 t e ta dard devatio o t e re e tve ara eter, e. . R , R , , a d A , a d d v d t e re ult by t e ea value o t e ara eter, t ereby v value o re ro du b l ty w re re e t t e 95 % o de e level, a arda e wt t e re o e dato ve SO/ EC Gu de 98-3⁴, a d w ay be d re ty o ar d wt t e ex a ded u erta ty value al ulated by alter atve et od .

**Table K.1 — Yeld tre t (,2% roo tre t or u eryeld tre t)—
Re ro du b l ty ro laboratory ter o ar o exer e
(ra re e tatio o t e value ve F ure K.1)**

Mater al	Code	Yeld tre t MPa	Re ro du b l ty ± %	Re ere e
Alu u				
S eet	AA5754	1 5,7	3,2	31
S eet	AA5182-O	126,4	1,9	2
S eet	AA6 16-T4	127,2	2,2	2
	EC-H 19	158,4	4,1	33
	2 24-T 351	362,9	3,	33
Steel				
S eet	DX56	162,	4,6	31
Low arbo , late	HR3	228,6	8,2	34
S eet	StE 18	267,1	9,9	31
A S 1 5	P245GH	367,4	5,	34
	C22	4 2,4	4,9	33
Plate	S355	427,6	6,1	31
Au te t S S	SS316L	23 ,7	6,9	31
Au te t S S	X2CrN 18-1	3 3,8	6,5	34
Au te t S S	X2CrN Mo18-1	353,3	7,8	34
A S 316	X5CrN Mo17-12-2	48 ,1	8,1	33
Marte t S S	X12Cr13	967,5	3,2	33
H Stre t	3 NCrMo16	1 39,9	2,	34
N kel alloy				
NCONEL 6	N Cr15Fe8	268,3	4,4	33
N o 75	(BCR-661)	298,1	4,	29
N o 75	(BCR-661)	3 2,1	3,6	31



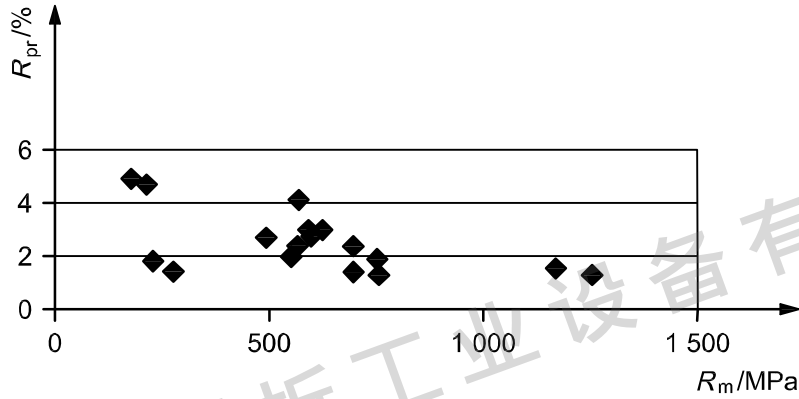
Key

R_{eH} upper yield strength
 R_p proof strength
 R_{pr} reproducibility

Figure K.1 — Pre-evaluation of Table K.1

Table K.2 — Tensile strength, R_p — Reproducibility for laboratory test or exercise (reference value from Figure K.2)

Material	Code	Tensile strength MPa	Reproducibility \pm %	Reference
Aluminum				
Sheet	AA5754	212,3	4,7	31
Sheet	AA5182	275,2	1,4	2
Sheet	AA616-T4	228,3	1,8	2
	EC-H 19	176,9	4,9	33
	2024-T 351	491,3	2,7	33
Steel				
Sheet	DX56	311	5,	31
Low carbon, plate	HR3	335,2	5,	34
Sheet	StE 18	315,3	4,2	31
AS 15	Fe51 C	552,4	2,	34
	C22	596,9	2,8	33
Plate	S355	564,9	2,4	31
Austenitic SS	SS316L	568,7	4,1	31
Austenitic SS	X2CrN 18-1	594,	3,	34
Austenitic SS	X2CrN Mo18-1	622,5	3,	34
AS 316	X7CrN Mo17-12-2	694,6	2,4	33
Martensitic SS	X12Cr13	1253,	1,3	33
High strength	3 N CrMo16	1167,8	1,5	34
Nickel alloy				
INCONEL 6	N Cr15Fe8	695,9	1,4	33
Ni 75	(BCR-661)	749,6	1,9	29
Ni 75	(BCR-661)	754,2	1,3	31



Key

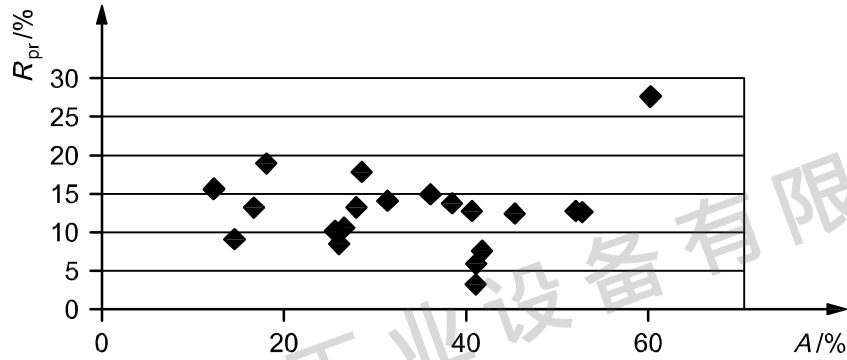
R_m — tensile strength
 R_{pr} — reproducibility

Figure K.2 — Pre-evaluation of data from Table K.2

Table K.3 — Elongation at fracture — Reproducibility of laboratory test results (relative evaluation of data from Figure K.3)

Material	Code	Elongation at fracture <i>A</i> %	Reproducibility \pm % ^a	Reference
Aluminum				
Sheet	AA5754	27,9	13,3	31
Sheet	AA5182-	26,6(<i>A₈</i>)	1,6	2
Sheet	AA616-T4	25,9(<i>A₈</i>)	8,4	2
	EC-H 19	14,6	9,1	33
	2024-T 351	18,	18,9 ^a	33
Steel				
Sheet	DX56	45,2	12,4	31
Low carbon, plate	HR3	38,4	13,8	34
Sheet	1E 18	4,5	12,7	31
AS 15	Fe51 C	31,4	14,	34
	C22	25,6	1,1	33
Plate	S355	28,5	17,7	31
Austenitic SS	SS316L	6,1	27,6	31
Austenitic SS	X2CrN 18-1	52,5	12,6	34
Austenitic SS	X2CrN Mo18-1	51,9	12,7	34
AS 316	X5CrN Mo17-12-2	35,9	14,9	33
Martensitic SS	X12Cr13	12,4	15,5	33
High strength	3 NCrMo16	16,7	13,3	34
Nickel alloy				
INCONEL 6	N Cr15Fe8	41,6	7,7	33
Ni 75	(BCR-661)	41,	3,3	29
Ni 75	(BCR-661)	41,	5,9	31

^a The reproducibility is expressed as a percentage of the average value of *A* of the test material; for 2024-T 351 aluminum the absolute value of *A* is (18, \pm 3,4) %.



Key

A elongation at break

R_p proof stress

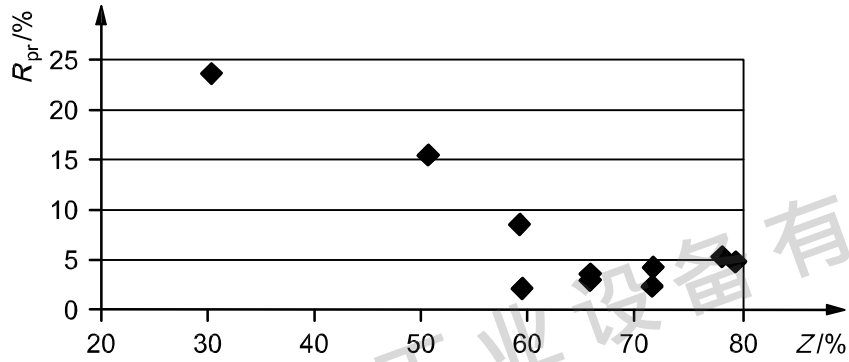
Figure K.3 — Proof stress versus elongation at break

Table K.4 — Reduction of area — Proof stress for laboratory test or exercise (reference value versus Figure K.4)

Material	Code	Reduction of area %	Proof stress \pm % ^a	Reference
Aluminum				
	EC-H 19	79,1	5,1	33
	2 24-T 351	3,3	23,7 ^b	33
Steel				
Low carbon, plate	HR3			
AS 15	Fe51 C	71,4	2,7	34
	C22	65,6	3,8	33
Austenitic SS	X2CrN 18-1			
Austenitic SS	X2CrN Mo18-1	77,9	5,6	34
AS 316	X5CrN Mo17-12-2	71,5	4,5	33
Martensitic SS	X12Cr13	5,5	15,6 ^b	33
High strength	3 NCrMo16	65,6	3,2	34
Nickel alloy				
NICONEL 6	NCr15Fe8	59,3	2,4	33
Ni 75	(BCR-661)	59,	8,8	29

^a The proof stress exercise data are taken from the test value of the reference material; for the 2 24-T 351 aluminum the absolute value of $(3,3 \pm 7,2)$ %.

^b So the value of proof stress may appear to be relatively low; this value is probably due to the relatively low yield strength of the material tested at room temperature. For the test of the material the yield strength of the material may be lower. The test value of the material is the yield strength of the material tested at room temperature.



Key
R_{pr} reproducibility
redu to o area

Figure K.4 — Pre e tat o o t e value ve Table K.4

Bibliography

- 1 SO 3183, *Petroleum and natural gas tubes — Steel and other materials*
- 2 SO 1196, *Petroleum and natural gas tubes — Steel and other materials for tubular well*
- 3 SO/TR 25679, *Material test methods — Symbols and designations of materials*
- 4 SO/EC Guide 98-3, *Ultrasonic testing — Part 3: Guide to the execution of ultrasonic testing (GUM:1995)*
- 5 SO/TTA 2, *Temperature distortion of ultrasonic test methods*
- 6 ASTM A37, *Standard test methods for ordinary carbon steel rods*
- 7 ASTM E8M, *Standard test methods for tensile testing of steel*
- 8 ASTM E112, *Standard methods for grain size analysis and determination of average grain size*
- 9 CWA 15261-2:2005, *Measurement of ultrasonic test methods — Test evaluation of ultrasonic test methods*
- 10 DN 5125, *Tensile test methods — Test methods*
- 11 EN 1291, *Metallurgical — Ultrasonic test methods — Method of test*
- 12 GB/T 228, *Metallurgical — Test methods at ambient temperature*
- 13 ACS W2, *Test methods for electrodeposited rod electrodeposits: Requirements for electrodeposited welds, W2-1 to W2-1.1. Test method A of the Classification Society, London, 2003. Available (2008-06-26) at: http://www.aenor.uk/document/ubl/ublato/uledrequiret/durw_d159.d*
- 14 JS 221, *Test methods for tensile test methods*
- 15 NS 8:1994, *Guide to the execution of ultrasonic test methods*
- 16 NS 33:1995, *Test methods for ultrasonic testing of electrodeposited*
- 17 DEAN, G.D., LOEDAY, M.S., COOPER, P.M. *Electrodeposited materials: DYSON, B.G., LOEDAY, M.S., GEE, M.G., editor. Material technology standards for tubular corrosion, 1952-1995. Cassell & Hall, London, 1995*
- 18 ROEBUCK, B., LORD, J.D., COOPER, P.M., MCCARTNEY, L.N. *Data available for the determination of ultrasonic test methods. J. Test. Eval. 1994, 22(1), 63-69*
- 19 SONNE, H.M., B. HESSE, B. *Determination of the ultrasonic test methods by ultrasonic test methods — Comparison of the test methods. Proceedings of the Werkstoff Material test 1993. D M, Berlin*
- 20 AEGERTER, J., KELLER, S., WESER, D. *Prüfung zur Durierung und Auswertung der Ultraschallprüfung für Al-Werkstoffe Test methods for the ultrasonic testing of aluminium alloys, Proceedings of the Werkstoff Material test 2003, 139-151. Stuttgart, Düsseldorf*

- 21 R DES, M., LORD, J. *TENSTAND al re ort: Co uter- o trolled te le te t a ord to EN 1 2-1: Re ult o a o ar o te t ro ra e to valdate a ro o al ora a e d e t o t e ta dard.* Nato al P y al Laboratory, Tedd to , 2 5
- 22 LORD, J. LO EDAY, M.S., R DES, M., MCENTAGGART, . *TENSTAND WP2 al re ort: D tal te le o tware evaluat o : Co uter- o trolled te le te t a e valdat o o Euro ea Sta dard EN 1 2-1.* Nato al P y al Laboratory, Tedd to , 2 5. 68 .
- 23 TAYLOR, B.N., KUYATT, C.E. *Gudel e or evaluat a d ex re t e u erta ty o NST ea ure e t re ult .* NST, Gat er bur , MD, 1994. 25 . (NST Te al Note 1297.) Ava lable (2 9- 7-23) at: [tt :// y . t. ov/Pub / udel e /TN1297/t 1297 . d](http://www.nst.gov/pub/udel/e/TN1297/t1297.d)
- 24 LO EDAY, M.S. *Roo te erature te le te t : A et od ore t at u erta ty o ea ure e t.* Nato al P y al Laboratory, Tedd to , 1999. *Mea ure e t ote CMMT (MN) 48.* Ava lable (2 9- 7-23) at: [tt :// ubl ato . l. o.uk/ l web/ d / t 48. d](http://www.npl.co.uk/1web/d/t48.d)
- 25 BELL, S.A. (1999) *A be er' ude to u erta ty o ea ure e t, 2 d ed to .* Nato al P y al Laboratory, Tedd to , 2 1. 41 . (*Mea ure e t Good Pra t e Gude*, No.11.) Ava lable (2 9- 7-31) at: [tt :// ubl ato . l. o.uk/ l web/ d / 11. d](http://www.npl.co.uk/1web/d/t11.d)
- 26 BRCH, K. *E t at u erta te te t .* Nato al P y al Laboratory, Tedd to , 2 1. (*Mea ure e t Good Pra t e Gude*, No.36.) Ava lable (2 9- 7-23) at: [tt :// ubl ato . l. o.uk/ l web/ d / 36. d](http://www.npl.co.uk/1web/d/t36.d)
- 27 KAND L, F.A., LORD, J.D., BULLOUGH, C.K., GEORGSSON, P., LEGENDRE, L., MONEY, G., MULL GAN, E., FRY, A.T., GORLEY, T.A.E., LAWRENCE, K.M. *T e UNCERT a ual o ode o ra t e or t e deter ato o u erta te e a al te t o etall ateral CD-ROM.* EC, Bru el
- 28 SONNE, H.M., KNAUF, G., SCHM DT- NGES, J. *Überle u e zur Über rü u vo u rü a e ttel Re ere z ateral Co derato o t e exa ato o our e te t equ e t by ea o re ere e ateral . : Pro eed o Werk to rü u Mater al te t 1996.* Bad Nau e . D M, Berl
- 29 NGELBRECHT, C.D., LO EDAY, M.S. *T e ert ato o a be t te erature te le ro rte o a re ere e ateral or te le te t a ord to EN 1 2-1: CRM 661.* EC, Bru el , 2 . (BCR Re ort EUR 19589 EN.)
- 3 L, H.-P., HOU, X. *New Co derato o t e u erta ty evaluato wt ea ured value o teel eet te le te t . : Metallur al a aly , 12t A ual Co ere e o A aly Te to C e e So ety or Metal , 2 4*
- 31 KL NGELHÖFFER, H., LEDWORUSK, S., BROOKES, S., MAY, T. *Co uter o trolled te le te t a ord to EN 1 2-1— Re ult o a o ar o te t ro ra e to valdate a ro o al ora a e d e t o t e ta dard— F al re ort o t e Euro ea ro e t TENSTAND— Work Pa ka e 4.* Bu de a talt ür Mater al or u u d - rü u (BAM), Berl , 2 5. 44 . (*For u ber t Te al re ort 268.*) Ava lable (2 8- 7- 1) at: [tt ://www.ba .de/de/ erv el/ ublkat o e / ublkat o e ede / b268 vt. d](http://www.bam.de/de/erv/el/ublkat/e/ublkato/e/ede/b268.vt.d)
- 32 LO EDAY, M.S., GRAY, T., AEGERTER, J. *Te le te t o etall ateral — A review— F al re ort o t e TENSTAND ro e t o work a ka e 1.* Bu de a talt ür Mater al or u u d - rü u (BAM), Berl , 2 4
- 33 ASTM Re ear Re ort E 28 1 4:1994, *Rou d rob re ult o terlaboratory te le te t*
- 34 ROESCH, L., COUE, N., TAL, J., D FANT, M. *Re ult o a terlaboratory te t ro ra e o roo te erature te le ro rte — Sta dard dev ato o t e ea ured value . (R S D Re ort, NDT 9331 .)*

- 35 LO EDAY, M.S. Toward a te le re ere e ateral. : LO EDAY, M.S., GBBONS, T.B. *Har o ato o te t ra t e or te erature ateral* , . 111-153. El ever, Lo do
- 36 JOHNSON, R.F., MURRAY, J.D. T e e e to rate o tra o t e .2 % roo tre a d lower yeld tre o teel. : Pro eed o Sy o u o H Te erature Per or a e o Steel , Ea tbour e, 1966. ro a d Steel t tute, 1967
- 37 GRAY, T.G.F., SHARP, J. lue e o a e ty e a d tra rate tera to te o te t . : PAPRNO, R., WESS, H.C. *Fa tor t ata e t t e re o o e a al te t* . ASTM, P ladel a, PA. (S e al Te al Publ ato 1 25.)
- 38 AEGERTER, J., BLOCH NG, H., SONNE, H.-M. lue e o t e t e t eed o t e yeld/ roo tre t — Te le te t o la ewt EN 1 2-1. *Material rü u 2 1, 1* , . 393-4 3
- 39 AEGERTER, J. Stra rate at a ve o t o a tre / tra urve t e te le te t ter al e ora du , AW Alu u , Bo , 2
- 40 BLOCH NG, H. *Cal ulato o t e e e ary ro ead velo ty / or a ev a e ed tre rate MPa/ Re ort. w k, UI* , 2 . 8 .
- 41 McENTEGGART, ., LOHR, R.D. Me a al te t a e r tera. : DYSON, B.G., LO EDAY, M.S., GEE, M.G., ed tor . *Material etrolo ya d ta dard or trutural er or a e* , . 19-33. Ca a & Hall, Lo do , 1995

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